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Beach Energy Artisan-1 Exploration Well

Oil Spill Modelling



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Terms and Abbreviations

0	Degrees	
•	Minutes	
"	Seconds	
Actionable oil	Oil which is thick enough for effective use of mitigation strategies, such as mechanical clean up (e.g. skimmers), booms, dispersed, or burned	
AMP	Australian marine parks	
AMSA	Australian Maritime Safety Authority	
ANZECC	Australian and New Zealand Environment and Conservation Council	
API	American Petroleum Institute gravity (A measure of how heavy or light a petroleum liquid in comparison to water)	
ASTM	American Society for Testing and Materials	
Bonn Agreement Oil Appearance Code	An agreement for cooperation in dealing with pollution of the North Sea by oil and other harmful substances, 1983, includes: Governments of the Kingdom of Belgium, the Kingdom of Denmark, the French Republic, the Federal Republic of Germany, the Republic of Ireland, the Kingdom of the Netherlands, the Kingdom of Norway, the Kingdom of Sweden, the United Kingdom of Great Britain and Northern Ireland and the European Union	
°C	Degree Celsius (unit of temperature)	
cP	Centipoise (unit of viscosity)	
CFSR	Climate Forecast System Reanalysis	
cm	Centimetre (unit of length)	
Decay	The process where oil components are changed either chemically or biologically (biodegradation) to another compound. It includes breakdown to simpler organic carbon compounds by bacteria and other organisms, photo-oxidation by solar energy, and other chemical reactions	
Dissolved hydrocarbons	Dissolved hydrocarbons within the water column with alternating double and single bonds between carbon atoms forming rings, containing at least one six-membered benzene ring	
g/m ²	Grams per square meter (unit of surface or area density)	
EIA	Environmental impact assessment	
Entrained oil	Droplets or globules of oil that are physically mixed (but not dissolved) into the water column. Physical entrainment can occur either during pressurised release from a subsurface location, or through the action of breaking waves (>12 knots)	
EP	Environmental plan	
EEZ	Exclusive Economic Zone	
Evaporation	The process whereby components of the oil mixture are transferred from the sea-surface to the atmosphere	
GODAE	Global Ocean Data Assimilation Experiment	
НҮСОМ	Hybrid Coordinate Ocean Model is a data-assimilative, three-dimensional ocean model	
HYDROMAP	Advanced ocean/coastal tidal model used to predict tidal water levels, current speed and current direction	
IOA	Index of Agreement gives a non-dimensional measure of model accuracy or performance	
IBRA	Interim Biogeographic Regionalisation for Australia	

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IMCRA	Integrated Marine and Coastal Regionalisation of Australia
Isopycnal layers	Water column layers with corresponding water densities
ITOPF	The International Tanker Owners Pollution Federation
KEF	Key Ecological Feature
km	Kilometre (unit of length)
km ²	Square Kilometres (unit of area)
KEF	Key ecological feature
Knot	unit of wind speed (1 knot = 0.514 m/s)
LGA	Local Government Area
LOWC	Loss of Well Control
m	Metres (unit of length)
m ²	Metres squared (unit of area)
m ³	Metres cubed (unit of volume)
m/s	Metres per Second (unit of speed)
MAE	Mean Absolute Error is the average of the absolute values of the difference between model predicted and observed data (e.g. surface elevations)
MB	Marine boundary
MNP	Marine National Park
RSB	Reefs, Shoals and Banks
MS	Marine Sanctuary
NASA	National Aeronautics and Space Administration
NCEP	National Centres for Environmental Prediction
NOAA	National Oceanic and Atmospheric Administration
NOPSEMA	National Offshore Petroleum Safety and Environmental Management Authority
nm	nautical mile (unit of distance; 1 nm = 1.852 km)
NP	National Parks
Ocean current	Large scale and continuous movement of seawater generated by forces such as breaking waves, wind, the Coriolis effect, and temperature and salinity gradients. It is the main flow of ocean waters
OECD	Organisation for Economic Co-operation and Development
ppb	Parts per billion (concentration)
ppb.hrs	ppb multiplied for hours (concentration x time)
PSU	Practical salinity units
Ramsar site	A wetland site designated of international importance under the Ramsar Convention
Ramsar Convention	The Convention on Wetlands, called the Ramsar Convention, is an intergovernmental treaty that provides the framework for national action and international cooperation for the conservation and wise use of wetlands and their resources.
Sea surface exposure	Floating oil on the sea surface equal to or above reporting threshold (e.g. 0.5 g/m ²)
Shoreline contact	Stranded oil on the shoreline equal to or above reporting threshold (e.g. 10 g/m ²)



SIMAP	Spill Impact Mapping Analysis Program
US EPA	United States Environmental Protection Agency
Visible oil	Floating oil on the sea surface equal to or above reporting threshold (e.g. 0.5 g/m ²)



EXECUTIVE SUMMARY

Background

Beach Energy is intending to undertake further development of the Otway offshore natural gas reserves. The proposed development will include the drilling of offshore exploration wells situated in the Otway Basin, starting with the Artisan-1 gas well. In order to support the development of environmental approvals for the drilling program, a comprehensive oil spill modelling study was commissioned which considered the following two hypothetical spill scenarios:

- 300 m³ surface release of marine diesel over 6 hours in the event of a containment loss from a vessel at the Artisan-1 well location; and
- 222,224 bbl subsea release of condensate over 86 days to represent an unrestricted open-hole loss of well control (LOWC) event from the Artisan-1.

SIMAP's (Spill Impact Mapping Analysis Program) stochastic model was used to quantify the probability of exposure from a spill to the sea (surface and in-water), and the probability of shoreline contact from hypothetical spill scenarios. The SIMAP system and the methods and analysis presented herein, use modelling algorithms which have been peer reviewed and published in international journals. Further, RPS warrants that this work meets and exceeds the ASTM Standard F2067-13 "*Standard Practice for Development and Use of Oil Spill Models*".

Methodology

The modelling study was carried out in several stages. Firstly, a five-year current dataset (2008–2012) that includes the combined influence of three-dimensional ocean and tidal currents was developed. Secondly, the currents, spatial winds and then detailed hydrocarbon properties were used as inputs in the oil spill model to simulate the drift, spread, weathering, entrainment and fate of the spilled hydrocarbons.

As spills can occur during any set of wind and current conditions, a total of 100 spill trajectories per hypothetical spill scenario per season (e.g. summer and winter) were initiated at random times within a 5-year period (2008–2012) to enable a robust statistical analysis.

Each simulation was configurated with the same spill information (i.e. spill volume, duration and oil type) except for the start time and date which in turns, ensures that the predicted transport and weathering of an oil slick is subject to a wide range of current and wind conditions.

Oil Properties

The marine diesel oil (MDO) used for Scenario 1, is a light-persistent fuel oil used in the maritime industry. It has a density of 829.1 kg/m³ (API of 37.6), a low pour point (-14°C) and low viscosity (4cP). According to the International Tankers Owners Pollution Federation (ITOPF, 2014) and AMSA (2015a) guidelines, this oil is categorised as a group II oil (light-persistent).

Thylacine condensate was used for the loss of well control scenario (Scenario 2). The condensate has an API of 44.3, density of 804.6 kg/m³ at 15°C) with low viscosity (0.875 cP), classifying it as a Group I oil according to the International Tankers Owners Pollution Federation (ITOPF, 2014) and USEPA/USCG classifications. The condensate comprises a significant portion of volatiles and semi to low volatiles (99% total) with very little residual components (<1%).



Key Findings

Scenario: 300 m³ surface release of marine diesel oil

Sea surface exposure

- No shoreline contact above the minimum threshold (>10 g/m²) was predicted for any of the seasons modelled.
- During summer conditions, low (0.5 g/m²) and moderate (10 g/m²) exposure to surface hydrocarbons were predicted to travel a maximum distance of 68 km and 12 km from the release location, respectively. During winter, low and moderate exposure of surface hydrocarbons extended to a maximum distance of 93 km and 10 km from the release location, respectively.
- The modelling results demonstrated a 1% probability of oil exposure on the sea surface for the Central Victoria Integrated Marine and Coastal Regionalisation of Australia (IMCRA) receptor, during the summer season.
- During winter conditions, there was a 1% probability of oil exposure on the sea surface for several receptors including the Central Victoria and Central Bass Strait IMCRA, Apollo Australian Marine Park (AMP) and within Victorian State Waters.
- None of the receptors were exposed at or above the moderate or high (>25 g/m²) thresholds with the
 exception of the Otway IMCRA. This receptor registered low, moderate and high exposure to sea
 surface hydrocarbons due to the release location being situated within the boundaries of this receptor.

Dissolved hydrocarbon exposure

- There was no dissolved hydrocarbon exposure (over the 48-hour window) in the 0-10 m depth layer to receptors at or above the low threshold (6 ppb), with the exception of the Otway IMCRA which registered 8 ppb and 9 ppb during summer and winter conditions, respectively. None of the receptors recorded exposure (over 48 hours) at or above the moderate (50 ppb) or high (400 ppb) thresholds.
- At the depths of 0-10 m, the dissolved hydrocarbon exposure over 1 hour was predicted for the Otway IMCRA, with the maximum concentration of 76 ppb during summer and 59 ppb during winter. No moderate or high dissolved hydrocarbons exposure (over 1 hour) was predicted for any receptors, except for the Otway IMCRA.

Entrained hydrocarbon exposure

- At the depths of 0-10 m, the maximum entrained hydrocarbon exposure (over a 48-hour window) during summer and winter conditions was 2,182 ppb and 792 ppb, respectively. None of the receptors were exposed at or above the moderate (10-100 ppb) or high (>1,000 ppb) thresholds, excluding the Otway IMCRA.
- Within the 0-10 m depth layer, the maximum entrained hydrocarbon exposure (over 1 hour) for the Otway IMCRA was 5,933 ppb and 5,046 ppb, during summer and winter conditions, respectively. For receptors other than the Otway IMCRA (83% summer and 93% winter), the probability of exposure to entrained hydrocarbons at or above the moderate threshold (100-1,000 ppb) ranged from 1% (Cape Patton sub-Local Government Area (sub-LGA)) to 8% (within Victorian State Waters) during summer conditions and 1% (Twelve Apostles Marine National Park (MNP)) to 16% (Apollo AMP) during winter conditions. No other receptors were exposed at or above the high threshold (>1,000 ppb), except for the Otway IMCRA.



Scenario: 222,224 bbl subsea release of condensate over 86 days

Sea surface exposure

- During summer conditions, low (0.5 -10 g/m²) and moderate (10 25 g/m²) exposure to surface hydrocarbons were predicted to travel a maximum distance of 52 km and 4 km from the release location, respectively. Under winter conditions, low and moderate exposure from surface hydrocarbons extended to a maximum distance of 53 km and 3 km from the release location, respectively. Note, no high exposure was predicted on the sea surface for any of the seasons assessed.
- During summer conditions, the probability of hydrocarbon exposure on the sea surface at or above the low threshold was predicted to range from 6% (Otway Ranges Interim Biogeographic Regionalisation for Australia (IBRA) sub-region) to 16% (Colac Otway and Cape Otway West sub-LGAs and within Victorian State Waters). The exception is the Otway IMCRA (100% during both seasons). The winter modelling results demonstrated a larger number of receptors exposed to surface hydrocarbons at or above the low threshold. The probability ranged from 3% (Twelve Apostles MNP and Otway Ranges IBRA) to 40% (Otway Plain IBRA; Cape Otway West sub-LGA and Colac Otway LGA). No other receptors except the Otway IMCRA were exposed to moderate or high levels for any seasons assessed.

Shoreline contact

- The probability of contact to any shoreline was 16% and 57% for the summer and winter season, respectively. While the minimum time for visible surface hydrocarbons to reach a shoreline was 3 days for 5 days, respectively.
- The maximum volume of hydrocarbons predicted to come ashore was 15 m³ and 33 m³, during summer and winter conditions, respectively, while the maximum length of shoreline contacted above the low threshold (10 – 100 g/m²) was 7.0 km and 11.0 km, respectively. Note, no shoreline loading was predicted for the high threshold (above 1,000 g/m²).
- Cape Otway West LGA was the receptor predicted with the greatest probability of contact above the low and moderate thresholds during summer (16% and 15%, respectively) and winter (40% for both thresholds) conditions. The modelling results during winter conditions demonstrated additional shoreline contact to Moyne, Corangamite, Moonlight head and Childers Cove.

In-water exposure

- At the depth of 0-10 m, the maximum concentration of dissolved hydrocarbons over the 48-hour window was 30 ppb in summer and 34 ppb in winter, and hence no moderate or high exposure was predicted during either season. For summer conditions, the probability of low exposure to dissolved hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF, Moyne LGA, Bay of Islands and Childers Cove sub-LGAs) to 17% (Otway Plain IBRA, Colac Otway LGA, Cape Otway West sub-LGA and within Victoria State Waters)The Otway IMCRA recorded a probability of 50% during summer. During winter conditions, the probability of low exposure to dissolved hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF, Bay of Islands and Lorne sub-LGA) to 16% (within Victoria State Waters). The Otway IMCRA registered a probability of 42% for winter. None of the receptors were exposed to moderate (50 400 ppb) or high (>400 ppb) dissolved hydrocarbons (over a 48-hour basis) during the summer or winter season.
- At the depths of 0-10 m, the maximum dissolved hydrocarbon concentrations predicted over the 1-hour period was 309 ppb during summer and 289 ppb for winter, which occurred within the Otway IMCRA and the Victoria State Waters. During summer conditions, the probability of moderate exposure to



dissolved hydrocarbons ranged from 1% (Glenelg Plain and Bridgewater IBRA's; Glenelg, Moyne and Surf Coast LGAs; Lorne, Bay of Islands, Childers Cove and Cape Nelson sub-LGAs) to 43% (Otway Plain IBRA, Colac Otway LGA, Cape Otway West sub-LGA and within Victoria State Waters). The probability for Otway IMCRA was 58%. Under winter conditions, the probability of moderate exposure (over 1 hour) to dissolved hydrocarbons ranged from 1% (Gippsland Plain IBRA; Flinders IMCRA; Point Addis and Wilsons Promontory MNP; Mornington Peninsula LGA; Lorne, Mornington Peninsula and Childers Cove sub-LGAs) to 57% for the Victorian State Waters. The probability of exposure to the Otway IMCRA was 68%. None of the receptors were exposed high concentrations during the summer or winter season.

- The maximum entrained hydrocarbon concentrations time-averaged over 48 hours for the summer and winter season was 559 ppb and 569 ppb, respectively. No moderate or high exposure was predicted for any of the receptors predicted for any of the seasons. During summer conditions, the probability of low exposure to entrained hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF; Moyne LGA; Bay of Islands and Childers Cove sub-LGAs) to 17% (Otway Plain IBRA; Colac Otway LGA; Cape Otway West sub-LGA and within Victorian State Waters), with the exception of IMCRA Otway (50%). During winter conditions, the probability of low exposure to entrained hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF; Bay of Islands and Lorne sub-LGAs) to 16% (Victoria State Waters), with the exception of Otway IMCRA (42%).
- Within the 0-10 m depth layer, the maximum concentration of entrained hydrocarbons over 1 hour was 948 ppb during summer and 932 ppb during winter, occurring within the Otway IMCRA. During summer conditions, the probability of moderate entrained hydrocarbon exposure ranged from 7% (Cape Patton sub-LGA) to 73% (Victorian State Waters). The probability of exposure to the Otway IMCRA receptor was 100% during both seasons. For other receptors during winter conditions, the probability of moderate entrained from 8% (along the shoreline of Childers Cove sub-LGA; Moyne and Warrnambool LGA) to 73% (within Victorian State Waters).



1 INTRODUCTION

Beach Energy¹ is seeking approval to undertake further development of the Otway offshore natural gas reserves. The proposed development will include the drilling of offshore exploration wells situated in the Otway Basin starting with the Artisan-1 gas exploration well. In order to obtain environmental approvals for the drilling program, Beach Energy commissioned RPS to undertake a comprehensive oil spill modelling based on the following two hypothetical spill scenarios:

- 300 m³ surface release of marine diesel over 6 hours in the event of a containment loss from a vessel at the Artisan-1 well location; and
- 222,224 bbl subsea release of condensate over 86 days to represent an unrestricted open-hole loss of well control (LOWC) event from the Artisan-1 well location.

Figure 1 and Table 1 present the location and coordinates of Artisan-1 which was used as the release location for the two scenarios.

The potential risk of exposure to the surrounding waters and contact to shorelines was assessed for summer (October to March) and winter (April to September) conditions. This approach assists with identifying the environmental values and sensitivities that would be at risk of exposure on a seasonal basis.

The purpose of the modelling is to further improve understanding of a conservative 'outer envelope' of the potential area that may be affected in the unlikely event of hydrocarbon release. The modelling does not take into consideration any of the spill prevention, mitigation and response capabilities that would be implemented in response to the spill. Therefore, the modelling results represent the maximum extent that the released hydrocarbon may influence.

The spill modelling was performed using an advanced three-dimensional trajectory and fates model; Spill Impact Mapping Analysis Program (SIMAP). The SIMAP model calculates the transport, spreading, entrainment and evaporation of spilled hydrocarbons over time, based on the prevailing wind and current conditions and the physical and chemical properties.

The hydrocarbon spill model, the method and analysis applied herein uses modelling algorithms which have been peer reviewed and published in international journals. Further, RPS warrants that this work meets and exceeds the American Society for Testing and Materials (ASTM) Standard F2067-13 "*Standard Practice for Development and Use of Oil Spill Models*".

			- I ²
Well location	Latitude	Longitude	Water Depth (m)

142° 52" 55.7' E

Table 1 Location of the Artisan-1 well location used for the oil spill modelling study.

38° 53" 29.4' S

Artisan-1

60

¹ It should be noted that Beach Energy is the 100% owner of Lattice Energy. Lattice Energy are the permit titleholder.

Report

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2 SCOPE OF WORK

The scope of work included the following components:

- 1. Generate tidal current patterns of the region using the ocean/coastal model, HYDROMAP;
- Use HYCOM (Hybrid Coordinate Ocean Model) ocean currents combined with HYDROMAP tidal currents over a 5-year period (2008 to 2012) to account for large scale flows offshore and tidal flows nearshore;
- 3. Use 5 years of high-resolution wind, aggregated current data and oil characteristics as input into the 3dimensional oil spill model SIMAP to represent the movement, spreading, entrainment, weathering of the oil over time; and
- 4. Use SIMAP's stochastic model (also known as a probability model) to calculate exposure to surrounding waters (sea surface and water column) and shorelines; and
- 5. Undertake a high-level deterministic analysis of the "worst case" LOWC scenario.



3 REGIONAL CURRENTS

Bass Strait is a body of water separating Tasmania from the southern Australian mainland, specifically the state of Victoria. The strait is a relatively shallow area of the continental shelf, connecting the southeast Indian Ocean with the Tasman Sea. Currents within the straight are primarily driven by tides, winds, incident continental shelf waves and density driven flows; high winds and strong tidal currents are frequent within the area (Jones, 1980).

The Otway Basin is part of the western field of the Bass Strait and lies along a north-west to south-east axis. It is approximately 500 km long and extends from Cape Jaffa in South Australia to north-west Tasmania and forms part of the Australian Southern Rift System.

The varied geography and bathymetry of the region, in addition to the forcing of the south-eastern Indian Ocean and local meteorology lead to complex shelf and slope circulation patterns (Middleton & Bye, 2007). Figure 2 displays seasonal surface current trends within the Bass Strait. During winter there is a strong eastward water flow due to the strengthening of the South Australian Current (fed by the Leeuwin Current in the Northwest Shelf), which bifurcates with one extension moving though the Bass Strait, and another forming the Zeehan Current off western Tasmania (Sandery & Kampf 2007). During summer, water flow reverses off Tasmania, King Island and the Otway Basin travelling eastward in offshore waters.

To accurately describe the variability in currents between the inshore and offshore region, a hybrid regional dataset was developed by combining deep ocean predictions obtained from HYCOM (Hybrid Coordinate Ocean Model) with 2-dimensional tidal currents developed by RPS. The following sections provide a summary of the hybrid regional data set.







3.1 Tidal Currents

Tidal current data was generated using RPS's advanced ocean/coastal model, HYDROMAP. The HYDROMAP model has been thoroughly tested and verified through field measurements throughout the world over the past 32 years (Isaji & Spaulding, 1984; Isaji, et al., 2001; Zigic, et al., 2003). HYDROMAP tidal current data has been used as input to forecast (in the future) and hindcast (in the past) pollutant spills in Australian waters and forms part of the Australian National Oil Spill Emergency Response System operated by AMSA (Australian Maritime Safety Authority).

HYDROMAP employs a sophisticated sub-gridding strategy, which supports up to six levels of spatial resolution, halving the grid cell size as each level of resolution is employed. The sub-gridding allows for higher resolution of currents within areas of greater bathymetric and coastline complexity, and/or of particular interest to a study.

The numerical solution methodology follows that of Davies (1977a and 1977b) with further developments for model efficiency by Owen (1980) and Gordon (1982). A more detailed presentation of the model can be found in Isaji and Spaulding (1984) and Isaji et al. (2001).

3.1.1 Grid Setup

The tidal model domain has been sub-gridded to a resolution of 500 m for shallow and coastal regions, starting from an offshore (or deep water) resolution of 8 km. The finer grids were allocated in a step-wise fashion to more accurately resolve flows along the coastline, around islands and over regions with more complex bathymetry. Figure 3 shows the tidal model grid covering the study domain.

A combination of datasets were used and merged to describe the shape of the seabed within the grid domain (Figure 4). These included spot depths and contours which were digitised from nautical charts released by the hydrographic offices as well as Geoscience Australia database and depths extracted from the Shuttle Radar Topography Mission (SRTM30_PLUS) Plus dataset (see Becker et al., 2009).





Figure 3 Sample of the model grid used to generate the tidal currents for the study region. Higher resolution areas are shown by the denser mesh.



Figure 4 Bathymetry defined throughout the tidal model domain.



3.1.2 Tidal Conditions

The ocean boundary data for the regional model was obtained from satellite measured altimetry data (TOPEX/Poseidon 7.2) which provided estimates of the eight dominant tidal constituents at a horizontal scale of approximately 0.25 degrees. The eight major tidal constituents used were K_2 , S_2 , M_2 , N_2 , K_1 , P_1 , O_1 and Q_1 . Using the tidal data, surface heights were firstly calculated along the open boundaries, at each time step in the model.

The TOPEX/Poseidon satellite data has a global resolution of 0.25 degrees and is produced and quality controlled by NASA (National Aeronautics and Space Administration). The satellites equipped with two highly accurate altimeters and capable of taking sea level measurements with an accuracy of \pm 5 cm measured oceanic surface elevations (and the resultant tides) for over 13 years (1992–2005). In total, these satellites carried out 62,000 orbits of the planet.

The TOPEX/Poseidon tidal data has been widely used amongst the oceanographic community, being included in more than 2,100 research publications (e.g. Andersen, 1995; Ludicone et al., 1998; Matsumoto et al., 2000; Kostianoy et al., 2003; Yaremchuk and Tangdong, 2004; Qiu and Chen 2010). As such the TOPEX/Poseidon tidal data is considered suitably accurate for this study.

3.1.3 Surface Elevation Validation

To ensure that tidal predictions were accurate, predicted surface elevations were compared to data observed at five locations (see Figure 5).

To provide a statistical measure of the model performance, the Index of Agreement (IOA - Willmott (1981)) and the Mean Absolute Error (MAE - Willmott (1982) and Willmott and Matsuura (2005)) were used.

The MAE (Eq.1) is simply the average of the absolute values of the difference between the model-predicted (P) and observed (O) variables. It is a more natural measure of the average error (Willmott and Matsuura, 2005) and more readily understood. The MAE is determined by:

$$MAE = N^{-1} \sum_{i=1}^{N} |P_i - O_i|$$
 Eq.1

Where: N = Number of observations

 P_i = Model predicted surface elevation

 O_i = Observed surface elevation

The Index of Agreement (IOA; Eq. 2) in contrast, gives a non-dimensional measure of model accuracy or performance. A perfect agreement between the model predicted and observed surface elevations exists if the index gives an agreement value of 1, and complete disagreement between model and observed surface elevations will produce an index measure of 0 (Wilmott, 1981). Willmott et al (1985) also suggests that values larger than 0.5 may represent good model performance. The IOA is determined by:

$$IOA = 1 - \frac{\sum |X_{model} - X_{obs}|^2}{\sum (|X_{model} - \overline{X_{obs}}| + |X_{obs} - \overline{X_{obs}}|)^2}$$
Eq.2

Where: X_{model} = Model predicted surface elevation

X_{obs} = Observed surface elevation

Clearly, a greater IOA and lower MAE represent a better model performance.

Figure 6 and Figure 7 illustrate a comparison of the predicted and observed surface elevations for each location for January 2014. As shown on the graph, the model accurately reproduced the phase and amplitudes throughout the spring and neap tidal cycles. Table 2 shows the statistical comparison between the observed and predicted surface elevations. For all of the stations, the IOA is well within the limits



highlighting a good model performance. Hence, the tidal model predictions are considered accurate for this study.

Table 2	Statistical comparison between the observed and predicted surface elevations
---------	------------------------------------------------------------------------------

Tide Station	IOA	MAE (m)		
Gabo Island	0.98	0.08		
Port MacDonnell	0.98	0.05		
Port Welshpool	0.92	0.30		
Portland	0.97	0.07		
Gabo Island	0.96	0.22		



Figure 5 Tide stations used to calibrate surface elevation within the model.

Figure 8 is a snapshot of the predicted tidal current vectors.





Figure 6 Comparison between HYDROMAP predicted (blue line) and observed (red line) surface elevation at tidal stations Gabo Island (upper image), Port MacDonnell (middle image) and Port Welshpool (lower image).

RPS



Figure 7 Comparison between HYDROMAP predicted (blue line) and observed (red line) surface elevation at tidal stations Portland (upper image) and Stack Island (lower image).



Figure 8 Snapshot of the predicted tidal current vectors. Note the density of the tidal vectors vary with the grid resolution, particularly along the coastline and around the islands and sholas.



3.2 Ocean Currents

Data describing the flow of ocean currents was obtained from HYCOM (Hybrid Coordinate Ocean Model, (Chassignet et al., 2007), which is operated by the HYCOM Consortium, sponsored by the Global Ocean Data Assimilation Experiment (GODAE). HYCOM is a data-assimilative, three-dimensional ocean model that is run as a hindcast (for a past period), assimilating time-varying observations of sea surface height, sea surface temperature and in-situ temperature and salinity measurements (Chassignet et al., 2009). The HYCOM predictions for drift currents are produced at a horizontal spatial resolution of approximately 8.25 km (1/12th of a degree) over the region, at a frequency of once per day. HYCOM uses isopycnal layers in the open, stratified ocean, but uses the layered continuity equation to make a dynamically smooth transition to a terrain following coordinate in shallow coastal regions, and to z-level coordinates in the mixed layer and/or unstratified seas.

For this study, the HYCOM reanalysis hindcast currents were obtained for the years 2008 to 2012 (inclusive). Five years of data has been found to be suitably sufficient to account for the inter-annual variations and conditions with Bass Strait.

3.3 Surface Currents at the release site

Table 3 displays the predicted average and maximum surface current speed near the release location. Figure 9 and Figure 10 illustrate the monthly and seasonal current rose distributions (2008-2012 inclusive) derived from combining HYCOM ocean current data and HYDROMAP tidal data, respectively.

Note the convention for defining current direction throughout this report is the direction the current flows towards. Each branch of the current rose distribution represents the currents flowing to that direction, with north to the top of the diagram. The branches are divided into segments of different colour, which represent the current speed ranges for each direction. Speed intervals of 0.1 m/s are predominantly used in these current roses. The length of each coloured segment within a branch is proportional to the frequency of currents flowing within the corresponding speed and direction.

The combined current data (ocean plus tides) indicated that during April to December the currents predominately flowed east and west during January to March. Monthly average surface current speed was similar throughout the year (0.16 to 0.25 m/s), while the maximum surface current speed ranged between 0.60 m/s (November and January) and 1.22 m/s (July).



Table 3Predicted monthly average and maximum surface current speeds adjacent to the release
location. Data derived by combining the HYCOM ocean data and HYDROMAP high
resolution tidal data from 2008-2012 (inclusive).

Month	Average current speed (m/s)	Maximum current speed (m/s)	General direction (towards)	
January	0.17	0.60	WNW and ENE	
February	0.18	0.69	WNW	
March	0.16	0.85	WNW and ENE	
April	0.16	1.20	E	
Мау	0.16	0.78	E	
June	0.22	0.99	E	
July	0.22	1.22	E	
August	0.25	1.01	ESE	
September	0.22	0.90	E	
October	0.18	0.68	E	
November	0.17	0.60	E	
December	0.19	0.68	E	
Minimum	0.16	0.60		
Maximum	0.25	1.22	-	



RPS Data Set Analysis

Current Speed (m/s) and Direction Rose (All Records)



Longitude = 142.88°E, Latitude = 38.89°S Analysis Period: 01-Jan-2008 to 31-Jan-2012

Figure 9 Monthly surface current rose plots near the release location (derived by combining the HYDROMAP tidal currents and HYCOM ocean currents for 2008 – 2012 inclusive).



*Calm defined as < 0.01

RPS Data Set Analysis Current Speed (m/s) and Direction Rose (All Records)



Longitude = 142.88°E, Latitude = 38.89°S Analysis Period: 01-Jan-2008 to 31-Jan-2012

Figure 10 Seasonal surface current rose plots near the release location (derived by combining the HYDROMAP tidal currents and HYCOM ocean currents for 2008 – 2012 inclusive).



4 WIND DATA

High resolution wind data was sourced from the National Centre for Environmental Prediction (NCEP) Climate Forecast System Reanalysis (CFSR; see Saha et al., 2010) from 2008 to 2012 (inclusive). The CFSR wind model includes observations from many data sources; surface observations, upper-atmosphere air balloon observations, aircraft observations and satellite observations and is capable of accurately representing the interaction between the earth's oceans, land and atmosphere. The gridded wind data output is available at ¼ of a degree resolution (~33 km) and 1-hourly time intervals. Figure 11 shows the spatial resolution of the wind field used as input into the oil spill model. Table 4 shows the monthly average and maximum winds derived from the CFSR node located adjacent to the release site. Figure 12 and Figure 13 show the monthly and seasonal wind rose distributions, respectively.

Note the convention for defining wind direction throughout this report is the direction the wind blows from. Each branch of the wind rose distribution represents wind coming from that direction, with north to the top of the diagram. The branches are divided into segments of different colour, which represent wind speed ranges from that direction. Speed ranges of 3 knot intervals, excluding the calm and near calm conditions are used in these wind roses. The length of each coloured segment within a branch is proportional to the frequency of winds blowing within the corresponding range of speeds from that direction.

The wind data analysis indicated that winds in the region are generally moderate to strong throughout the year, with a monthly average oscillating between ~13 knots (March) to ~18 knots (August). A maximum wind speed of 49 knots was recorded during September, while the lowest maximum speed of 34 knots occurred in December.



Figure 11 Image showing the CFSR modelled wind nodes.



Table 4Predicted monthly average and maximum winds for the wind node adjacent to the
release location. Data derived from CFSR hindcast model from 2008-2012 (inclusive).

Month	Average wind (knots)	Maximum wind (knots)	General direction (from)	
January	13	37	Variable SW to SE	
February	14	37	SE	
March	13	38	Variable	
April	14	44	W	
Мау	13	36	W	
June	16	46	SW to NW	
July	18	44	SW to NW	
August	18	46	SW to NW	
September	17	49	SW	
October	14	35	SW to S	
November	14	38	W to SE	
December	14	34	W to E	
Minimum	13	34	_	
Maximum	18	49		



RPS Data Set Analysis Wind Speed (knots) and Direction Rose (All Records)



Longitude = 142.88°E, Latitude = 38.89°S Analysis Period: 01-Jan-2008 to 31-Jan-2012

Figure 12 Monthly wind rose distributions derived from the CFSR hindcast model from 2008–2012 (inclusive), for the nearest wind node to the release location.



RPS Data Set Analysis

Wind Speed (knots) and Direction Rose (All Records)

Longitude = 142.88°E, Latitude = 38.89°S Analysis Period: 01-Jan-2008 to 31-Jan-2012



Figure 13 Seasonal wind rose distributions derived from the CFSR hindcast model from 2008–2012 (inclusive), for the nearest wind node to the release location.



5 WATER TEMPERATURE AND SALINITY

The monthly depth-varying water temperature and salinity profiles at 5 m intervals through the water column adjacent to the release location (refer to Figure 14) was obtained from the World Ocean Atlas 2013 (WOA13) produced by the National Oceanographic Data Centre (National Oceanic and Atmospheric Administration) (see Levitus et al., 2013). The data is to inform the weathering, movement and evaporative loss of hydrocarbon spills in the surface and subsurface layers.

Table 5 summarises the monthly average sea surface temperatures and salinity (0-5 m depth layer). The sea surface temperatures were shown to range from 13.3°C (September) and 18.0°C (January). Salinity remained consistent throughout the year ranging from 35.1 to 35.6 psu.

Table 5Monthly average sea surface temperature and salinity in the 0–5 m depth layer near the
Artisan-1 well location.

Month	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Temperature (°C)	18.0	17.2	17.9	16.4	16.3	16.0	14.9	13.6	13.3	14.6	14.4	16.1
Salinity (psu)	35.4	35.1	35.4	35.4	35.4	35.4	35.6	35.3	35.3	35.4	35.4	35.4

Report





Figure 14 Monthly water temperature and salinity profiles near the release location.

RPS

6 NEAR-FIELD MODEL – OILMAP-DEEP

Near-field modelling was carried out for the loss of well control scenario to better understand the plume dynamics due to the amalgamation of condensate and gas at the seabed using the advanced OILMAP-DEEP blowout model. OILMAP-DEEP was developed by RPS and designed to provide the near-field behaviour of multi-phase gas-condensate plumes during subsurface blowout releases.

The model simulates the plume rise dynamics in two phases, the initial jet phase and the buoyant plume phase. The initial jet phase governs the plume dynamics directly above the subsea release location and is predominantly driven by the exit velocity. During this phase, the condensate droplet size and distribution are calculated. Next, the rise dynamics are dominated by the buoyant nature of the plume until the termination of the plume phase (known as the trapping depth). At this point, the results from OILMAP-DEEP (including plume trapping depth, plume diameter and droplet size distribution) are integrated into the far-field model SIMAP to simulate the rise and dispersion of the condensate droplets.

More details on the OILMAP-DEEP model, can be found in Spaulding et al. (2015). The model has been validated against observations from Deepwater Horizon as well as small and large-scale laboratory studies on subsurface oil releases (Brandvik et al 2013, 2014; Belore 2014; Spaulding et al. 2015; Li et al. 2017). Figure 15 illustrates the various stages of an example blowout plume.

Table 6 presents the input parameters and key results of the subsea modelling. Note that a depleting release rate illustrated in Figure 16 was used for the LOWC scenario, starting from 3,758 bbl/day on day 1 and decreasing to 1,718 bbl/day on day 86. The near-field modelling showed that in the event of a blowout from a well, the gas/liquid will propel the condensate upward from the seabed and the plume would rupture the sea surface. Due to the velocity of the plume, the model predicted droplet sizes would be relatively small, ranging from 100 to 400 μ m.

Input Variable	Value					
Scenario	86-day loss of well control					
Water depth (m)	60					
Tubing diameter (inch)	8.5"					
Condensate Rate (stb/day)	3,758 bbl (day 1) depleting to 1,718 bbl (day 86)					
Water Rate (stb/day)	189 bbl (day 1) depleting to 137 bbl (day 86)					
Gas Rate (scf/day)	290,000,000 scf (day 1) depleting to 132,000,000 scf (day 86)					
Gas to Condensate ratio (scf/bbl)	81,727 (average)					
Gas to Total Liquids ratio (scf/bbl)	76,868 (average)					
Reservoir temperature (°C)	93					
Release Pressure (psia)	2,583 (day 1) depleting to 256 (day 86)					
Key Results						
Plume execution depth (m)	Plume ruptures the sea surface					
Droplet Sizes	100 – 400 μm					

 Table 6
 Input characteristics and key results from the subsea modelling.




Figure 15 Example of a blowout plume illustrating the various stages of the plume in the water column (Source: Applied Science Associates, 2011).



Figure 16 Depleting release rate used for the LOWC scenario



7 OIL SPILL MODEL – SIMAP

Modelling of the fate of oil was performed using SIMAP. SIMAP is designed to simulate the fate and effects of spilled hydrocarbons for both the surface and subsurface releases (Spaulding et al. 1994; French et al. 1999; French-McCay, 2003; French-McCay, 2004; French-McCay et al. 2004).

SIMAP has been used to predict the weathering and fate of oil spills during and after major incidents including: Montara (Australia) well blowout August 2009 in the Timor Sea (Asia-Pacific ASA, 2010); Macondo (USA) well blowout April 2010 in the Gulf of Mexico; Bohai Bay (China) oil spill August 2011; and the pipeline oil spill July 2013 in the Gulf of Thailand

The SIMAP model calculates the transport, spreading, entrainment, evaporation and decay of surface hydrocarbon slicks as well as the entrained and dissolved oil components in the water column, either from surface slicks or from oil discharged subsea. The movement and weathering of the spilled oil is calculated for specific oil types. Input specifications for oil mixtures include the density, viscosity, pour point, distillation curve (volume lost versus temperature) and the aromatic/aliphatic component ratios within given boiling point ranges. The SIMAP model uses an interpolation scheme based on an area-weighting scheme of the four nearest points of the wind and currents from the oil particle location.

SIMAP is a 3D model that allows for various response actions to be modelled including oil removal from skimming, burning, or collection booms, and surface and subsurface dispersant application.

The SIMAP oil spill model includes advanced weathering algorithms, specifically focussed on unique oils that tend to form emulsions and/or tar balls. The weathering algorithms are based on 5 years of extensive research conducted in response to the Deepwater Horizon oil spill in the Gulf of Mexico (French et al., 2015).

Biodegradation is included in the oil spill model. In the model, SIMAP, degradation is calculated for the surface slick, deposited oil on the shore, the entrained oil and dissolved constituents in the water column, and oil in the sediments. For surface oil, water column oil, and sedimented oil a first order degradation rate is specified. Biodegradation rates are relatively high for hydrocarbons in dissolved state or in dispersed small droplets.

7.1 Stochastic Modelling

Stochastic oil spill modelling is created by overlaying a great number (often 100 hundred) simulated hypothetical oil spills (e.g. Figure 17). Stochastic modelling involves running numerous individual oil spill simulations using a range of prevailing wind and current conditions that are historically representative of the season of where the spill event may occur.

For the stochastic modelling presented herein, 100 spills for each of season were simulated and each using the same spill information (release location, spill volume, duration and oil type) but with varied start dates and times corresponding to the period represented by the available wind and current data. During each simulation, the model records whether any grid cells are exposed to any oil concentrations, the concentrations involved and the elapsed time before exposure. The results of all 100 oil spill simulations were analysed to determine the following statistics for every grid cell:

- Exposure load (concentrations and volumes);
- Minimum time before exposure;
- Probability of contact above defined concentrations;
- Volume of oil that may strand on shorelines from any single simulation;
- Concentration that might occur on sections of individual shorelines; and
- Exposure (concentration x duration of exposure) to entrained and dissolved hydrocarbons in the water column.



Exposure (concentration x duration of exposure) to entrained and dissolved hydrocarbons in the water column



Figure 17 Predicted movement of four single oil spill simulations predicted by SIMAP for the same scenario (left image). All model runs are overlain (shown as the stacked runs on the right) and the number of times that trajectories contact a given location at a concentration is used to calculate the probability.

7.2 Sea surface, Shoreline and In-Water Exposure Thresholds

The thresholds for the sea surface, shoreline and water column (entrained and dissolved hydrocarbons) is presented in Table 7 and their relationship to exposure, are presented in Sections 7.2.1 to 7.2.3. Supporting justifications of the adopted thresholds applied during the study and additional context relating to the area of influence are also provided. It is important to note that the thresholds are in line with the thresholds recommended in the NOPSEMA oil spill modelling bulletin April 2019

(<u>https://www.nopsema.gov.au/assets/Bulletins/A652993.pdf</u>), In some instances, slightly more conservative. For example, the low surface exposure of >0.5 g/m² was adopted in the study, while the NOPSEMA bulletin recommends 1 g/m².

Table 7Exposure and contact threshold values used for the Artisan-1 oil spill modelling study.

Level	Sea Surface Exposure (g/m²)	Shoreline Contact (g/m²)	Dissolved Hydrocarbon Concentration (ppb) [#]	Entrained Hydrocarbon Concentrations (ppb) [#]
Low	0.5	10	6	10
Moderate	10	100	50	100
High	25	1,000	400	1,000

[#]These thresholds were assessed for a) 1 hour exposure and b) 48-hour exposure windows. Both sets of results are provided in the result section(s).



7.2.1 Sea Surface Exposure Thresholds

The minimum sea surface reporting level for each spill simulation was 0.5 g/m^2 , which equates to an average thickness of approximately $0.5 \mu m$. Oil of this thickness is described as a rainbow to metallic sheen in appearance according to the Bonn Agreement Oil Appearance Code (Bonn Agreement, 2009, Table 8). This thickness is considered the minimum level for observing oil in the marine environment by the Australian Maritime Safety Authority (AMSA, 2015). Furthermore, this threshold is considered below levels which would cause environmental harm and it is more indicative of the areas perceived to be affected due to its visibility on the sea surface and potential to trigger temporary closures of areas (i.e. fishing grounds) as a precautionary measure.

Ecological impact has been estimated to occur at 10 g/m^2 (a film thickness of approximately 10 µm or 0.01 mm) according to French et al. (1996) and French-McCay (2009) as this level of fresh oiling has been observed to mortally impact some birds through adhesion of oil to their feathers, exposing them to secondary effects such as hypothermia. The appearance at this average thickness has been described as a metallic sheen (Bonn Agreement, 2009). Concentrations above 10 g/m^2 is also considered the lower actionable threshold, where oil may be thick enough for containment and recovery as well as dispersant treatment (AMSA, 2015).

Scholten et al. (1996) and Koops et al. (2004) indicated that at oil concentrations on the sea surface of 25 g/m² (or greater), would be harmful for all birds that have landed in an oil film due to potential contamination of their feathers, with secondary effects such as loss of temperature regulation and ingestion of oil through preening. The appearance of oil at this thickness is also described as metallic sheen (Bonn Agreement, 2009).

The sea surface reporting thresholds applied in this study were 0.5–10 g/m² (low), 10–25 g/m² (moderate) and above 25 g/m² (high) (Table 7).

Note that the higher threshold applied in this study falls below the thickness that would begin to present as patches of true oil colour (Table 8).

Figure 18 shows examples of the differences between oil colour and corresponding thickness on the sea surface. Hydrocarbons in the marine environment may appear differently due the ambient environmental conditions (wind and wave action).

Code Description Appearance		Layer Thickness Interval (g/m² or μm)	Litres per km ²
1	Sheen (silvery/grey)	0.04 - 0.30	40 – 300
2	Rainbow	0.30 – 5.0	300 - 5,000
3	Metallic	5.0 – 50	5,000 - 50,000
4	Discontinuous True Oil Colour	50 – 200	50,000 - 200,000
5	Continuous True Oil Colour	200 ->	200,000 ->

Table 8 Bonn Agreement Oil Appearance Code







The generic oil colour categories used in this report are meant as a guide only. For more accurate description of oil appearance on the sea surface a detailed analysis of an oil should be undertaken.

The specific oil type will determine appearance (i.e. colour) and behaviour on the sea surface. Lighter oils such as marine diesel and condensate, have true oil colours that are pale or transparent. As such, these oil types may not increase beyond a rainbow or metallic sheen, despite their thickness increasing beyond 25 g/m² (~25 um). Moreover, the physical properties and appearance of oil types will change due to weathering on the sea surface. For example, oils with high paraffinic wax content will form waxy sheets that break up into flakes or nodules after the more volatile components have evaporated. Take up of water by the oil (emulsification) will also significantly change the appearance and thickness of floating oil. Stable water-in-oil emulsions will have a higher combined mass and thickness and will present as thick, semi-solid, aerated layers that tend to be coloured strongly red/brown, orange or yellow, rather than the true oil colour.

It should be noted that in the case of solidified or emulsified oils, mass per area estimates cannot be directly referenced to the Bonn Agreement visibility scale that refers only to oil present as films or slicks of oil alone.

7.2.2 Shoreline Exposure Thresholds

The reporting threshold of 10 g/m² was applied as the visible limit for oil on shore. This threshold may trigger socio-economic impact, such as triggering temporary closures of beaches to recreation or fishing, or closure of commercial fisheries and might trigger attempts for shore clean-up on beaches or man-made features/amenities (breakwaters, jetties, marinas, etc.). In previous risk assessment studies, French-McCay et al (2005a; 2005b) used a threshold of 10 g/m², equating to approximately two teaspoons of oil per square meter of shoreline, as a low impact threshold when assessing the potential for shoreline exposure.

French et al. (1996) and French-McCay (2009) define a shoreline oil threshold of 100 g/m², or above, as having potentially harm shorebirds and wildlife (furbearing aquatic mammals and marine reptiles on or along the shore) based on studies for sub-lethal and lethal impacts. This threshold has been used in previous environmental risk assessment studies (see French-McCay, 2003; French-McCay et al., 2004, French-McCay et al., 2011, 2012; NOAA, 2013). Additionally, a shoreline concentration of 100 g/m², or above, is the minimum limit that the oil can be effectively cleaned according the AMSA (2015) guidelines. This threshold equates to approximately ½ a cup of oil per square meter of shoreline exposure. The appearance is described as a thin oil coat.

The higher threshold of 1,000 g/m², and above, was adopted to inform locations that might receive oil accumulation levels that could have a higher potential for ecological effect. Observations by Lin and Mendelssohn (1996), demonstrated that loadings of more than 1,000 g/m² of oil during the growing season



would be required to impact marsh plants significantly. Similar thresholds have been found in studies assessing oil impacts on mangroves (Grant et al., 1993; Suprayogi & Murray, 1999). This concentration equates to approximately 1 litre or 4 ¼ cups of fresh oil per square meter of shoreline exposure. The appearance is described as an oil cover.

The shoreline reporting thresholds applied in this study were $10-100 \text{ g/m}^2$ (low), $100-1,000 \text{ g/m}^2$ (moderate) and above $1,000 \text{ g/m}^2$ (high) (Table 7).

7.2.3 Dissolved and Entrained Hydrocarbon Thresholds

Oil is a mixture of thousands of hydrocarbons of varying physical, chemical, and toxicological characteristics, and therefore, demonstrate varying fates and impacts on organisms. As such, for in-water exposure, the SIMAP model provides separate outputs for dissolved and entrained hydrocarbons from oil droplets. The consequences of exposure to dissolved and entrained components will differ because they have different modes and magnitudes of effect.

Entrained hydrocarbon concentrations were calculated based on oil droplets that are suspended in the water column, though not dissolved. The composition of this oil would vary with the state of weathering (oil age) and may contain soluble hydrocarbons when the oil is fresh. Calculations for dissolved hydrocarbons specifically calculates oil components which are dissolved in water, which are known to be the primary source of toxicity exerted by oil.

7.2.3.1 Dissolved hydrocarbons

Laboratory studies have shown that dissolved hydrocarbons exert most of the toxic effects of oil on aquatic biota (Carls et al., 2008; Nordtug et al., 2011; Redman, 2015). The mode of action is a narcotic effect, which is positively related to the concentration of soluble hydrocarbons in the body tissues of organisms (French-McCay, 2002). Dissolved hydrocarbons are taken up by organisms directly from the water column by absorption through external surfaces and gills, as well as through the digestive tract. Thus, soluble hydrocarbons are termed "bioavailable".

Hydrocarbon compounds vary in water-solubility and the toxicity exerted by individual compounds is inversely related to solubility, however bioavailability will be modified by the volatility of individual compounds (Nirmalakhandan &Speece, 1988; Blum & Speece, 1990; McCarty, 1986; McCarty et al., 1992a, 1992b; Mackay et al., 1992; McCarty & Mackay, 1993; Verhaar et al., 1992, 1999; Swartz et al., 1995; French-McCay, 2002; McGrath et al., 2009). Of the soluble compounds, the greatest contributor to toxicity for water-column and benthic organisms are the lower-molecular-weight aromatic compounds, which are both volatile and soluble in water. Although they are not the most water-soluble hydrocarbons within most oil types, the polynuclear aromatic hydrocarbons (PAHs) containing 2-3 aromatic ring structures typically exert the largest narcotic effects because they are semi-soluble and not highly volatile, so they persist in the environment long enough for significant accumulation to occur (Anderson et al., 1974, 1987; Neff & Anderson, 1981; Malins & Hodgins, 1981; McAuliffe, 1987; NRC, 2003). The monoaromatic hydrocarbons (MAHs), including the BTEX compounds (benzene, toluene, ethylbenzene, and xylenes), and the soluble alkanes (straight chain hydrocarbons) also contribute to toxicity, but these compounds are highly volatile, so that their contribution will be low when oil is exposed to evaporation and higher when oil is discharged at depth where volatilisation does not occur (French-McCay, 2002).

French-McCay (2002) reviewed available toxicity data, where marine biota was exposed to dissolved hydrocarbons prepared from oil mixtures, finding that 95% of species and life stages exhibited 50% population mortality (LC_{50}) between 6 and 400 ppb total PAH concentration after 96 hrs exposure, with an average of 50 ppb. Hence, concentrations lower than 6 ppb total PAH value should be protective of 97.5% of species and life stages even with exposure periods of days (at least 96 hours). Early life-history stages of fish appear to be more sensitive than older fish stages and invertebrates.



Exceedances of time averaged exposure (based on 96 hours) at 6, 50 or 400 ppb was applied to indicate increasing potential for sub-lethal to lethal toxic effects (or low to high).

Furthermore, in accordance with the NOPSEMA oil spill modelling bulletin, the same thresholds were assessed over a 1 hour time step (see Table 7).

7.2.3.2 Entrained hydrocarbons

Entrained hydrocarbons consist of oil droplets that are suspended in the water column and insoluble. As such, insoluble compounds in oil cannot be absorbed from the water column by aquatic organisms, hence are not bioavailable through absorption of compounds from the water. Exposure to these compounds would require routes of uptake other than absorption of soluble compounds. The route of exposure of organisms to whole oil alone include direct contact with tissues of organisms and uptake of oil by direct consumption, with potential for biomagnification through the food chain (NRC, 2005).

The 10 ppb threshold represents the very lowest concentration and corresponds generally with the lowest trigger levels for chronic exposure for entrained hydrocarbons in the ANZECC (2000) water quality guidelines. Due to the requirement for relatively long exposure times (> 24 hours) for these concentrations to be significant, they are likely to be more meaningful for juvenile fish, larvae and planktonic organisms that might be entrained (or otherwise moving) within the entrained plumes, or when entrained hydrocarbons adhere to organisms or trapped against a shoreline for periods of several days or more.

This exposure zone is not considered to be of significant biological impact and is therefore outside the adverse exposure zone. This exposure zone represents the area contacted by the spill. This area does not define the area of influence as it is considered that the environment will not be affected by the entrained hydrocarbon at this level.

Thresholds of 10 ppb, 100 ppb and 500 ppb were applied as time averaged exposure (over 96 hours, see Table 7), to cover the range of thresholds outlined in the ANZECC/ARMCANZ (2000) water quality guidelines and the incremental change for greater potential effect.

A complicating factor that should be considered when assessing the consequence of dissolved and entrained oil distributions is that there will be some areas where both physically entrained oil droplets and dissolved hydrocarbons co-exist. Higher concentrations of each will tend to occur close to the source where sea conditions can force mixing of relatively unweathered oil into the water column, resulting in more rapid dissolution of soluble compounds.

Furthermore, in accordance with the NOPSEMA oil spill modelling bulletin, the same thresholds were assessed over a 1 hour time step (see Table 7).

7.3 Oil Properties

7.3.1 Marine Diesel Oil

Marine Diesel Oil (MDO) is a light-persistent fuel oil used in the maritime industry. It has a density of 829.1 kg/m³ (API of 37.6) and a low pour point (-14°C). The low viscosity (4 cP) indicates that this oil will spread quickly when released and will form a thin to low thickness film on the sea surface, increasing the rate of evaporation. According to the International Tankers Owners Pollution Federation (ITOPF, 2014) and AMSA (2015a) guidelines, this oil is categorised as a group II oil (light-persistent).

Table 9 details the physical properties of MDO, while Table 10 presents the boiling point ranges of the MDO used in this study.

Figure 19 illustrates the weathering graph for a 300 m³ release of MDO over 6 hours during three wind speeds. The 5, 10 and 15 knot wind speeds were selected given that breaking waves and in turn entrainment takes place between 10 - 12 knots. The results illustrate that the prevailing wind speeds can



and do influence the weathering and fate of the MDO. Under lower wind-speeds (5 knots), the MDO will remain on the surface longer, spread quicker, and in turn greater evaporation. Conversely, <u>sustained</u> stronger winds (>15 knots) will generate breaking waves at the surface, causing a higher amount of MDO to be entrained into the water column and reducing the amount available to evaporate.

7.3.2 Thylacine Condensate

Thylacine condensate was used for the loss of well control scenario (Scenario 2). The condensate has an API of 44.3, density of 804.6 kg/m³ at 15°C) with low viscosity (0.875 cP) (refer to Table 9), classifying it as a Group I oil according to the (ITOPF, 2014) and USEPA/USCG classifications. The condensate comprises a significant portion of volatiles and semi to low volatiles (99% total) with very little residual components (<1%) (refer to Table 10). This means that the majority of the condensate will evaporate readily when on the water surface, with a minimal amount of persistent components to remain on the water surface over time.

Figure 1 displays the weathering graph for a 24-hour release (3,758 bbl) of Thylacine condensate during three static wind speeds. The weathering graph shows rapid evaporation occurs during the first 24 hours (while the condensate is still being released) during all three wind speeds. Thylacine condensate is predicted to readily entrain into the water column under the higher wind speeds (10 and 15 knots). Due to the high volatility of the condensate, little is predicted to remain on the water surface after the spill ceases.

Characteristic	MDO	Thylacine Condensate
Density (kg/m³) at 15°C	829.1	804.6
API	37.6	44.3
Dynamic viscosity (cP) at 20°C	4	0.875
Pour Point (°C)	-14	-50
Wax content (%)	1	NA
Hydrocarbon property category	Group II	Group I
Hydrocarbon property classification	Light - Persistent	Non-persistent oil

Table 9 Physical properties of MDO and Thylacine condensate

Table 10 Boiling point ranges of MDO and Thylacine condensate

Characteristic		Persistent		
	Volatile	Semi-volatile	Low volatility	Residual
Boiling point (°C)	< 180	180 - 265	265 - 380	>380
MDO	6.0	34.6	54.4	5.0
Thylacine condensate	64.0	19.0	16.0	1





Figure 19 Weathering of a 300 m³ surface release of MDO over 6 hours (tracked for 30 days) under three static winds conditions (5, 10 and 15 knots).





Figure 1 Weathering of 3,758 bbl subsea release of Thylacine condensate over 24 hours (tracked for 30 days) under three static wind speeds (5,10 and 15 knots).



7.4 Model Settings

This oil spill modelling study quantified the seasonal risk and potential exposure to the surrounding waters and shorelines for two plausible, yet hypothetical scenarios:

- 300 m³ surface release of marine diesel over 6 hours in the event of a containment loss from a vessel at the Artisan-1 well location; and
- 222,224 bbl subsea release of condensate over 86 days to represent an unrestricted open-hole loss of well control (LOWC) event from the Artisan-1 well location

Table 11 provides a summary of the oil spill model settings.

Parameter	Oil Spill Scenario					
Scenario description	Subsea Loss of Well Control	Loss of Containment from a Vessel				
Model period	Summer (October to March) Winter (April to September)					
Number of randomly selected spill start times and locations per season	100 (200 total)	100 (200 total)				
Oil type	Thylacine condensate	MDO				
Spill volume	222,224 bbl	300 m ³				
Release type	Subsea (60m)	Surface				
Release duration	86 days	6 hr				
Simulation length (days)	114	30				
Surface oil concentration thresholds	0.5 g/m², ′	10 g/m², >25 g/m²				
Shoreline load threshold	10 g/m², 100) g/m², >1,000 g/m²				
Dissolved hydrocarbon exposure to assess the potential exposure (ppb). These thresholds were assessed for 1 hour and 48-hour exposure windows.	6 ppb, potential low exposure 50 ppb, potential moderate exposure 400 ppb, potential high exposure					
Entrained hydrocarbon exposure to assess the potential exposure (ppb). These thresholds were assessed for 1 hour and 48-hour exposure windows.	10 ppb, potential low exposure 100 ppb, potential moderate exposure 1,000 ppb, potential high exposure					

Table 11 Summary of the oil spill model settings



8 PRESENTATION AND INTERPRETATION OF MODEL RESULTS

The results from the modelling study are presented in a number of statistical tables, which aim to provide a comprehensive understanding of the predicted sea-surface and in-water (subsurface) exposure and shoreline contact (if predicted).

8.1 Seasonal Analysis

The seasonal analysis is presented in the form of statistical tables based on the following principles:

- The <u>greatest distance travelled by a spill trajectory</u> is determined by a) recording the maximum and b) second greatest distance travelled (or 99th percentile) by a single trajectory, within a scenario, from the release location to the identified exposure thresholds.
- The <u>probability of shoreline contact</u> is determined by recording the number of spill trajectories to contact the shoreline, at a specific threshold, divided by the total number of spill trajectories within that scenario.
- The <u>minimum time before oil exposure</u> is determined by recording the minimum time for a grid cell to record exposure, at a specific threshold.
- The <u>average volume of oil ashore for a single spill</u> is determined by calculating the average volume of the all the single spill trajectories which were predicted to make shoreline contact within a scenario.
- The <u>maximum volume of oil ashore from a single spill trajectory</u> is determined by identifying the single spill trajectory within a scenario/season, that recorded the maximum volume of oil to come ashore and presenting that value.
- The <u>average length of shoreline contacted by oil</u> is determined by calculating the average of the length of shoreline (measured as grid cells) contacted by oil above a specified threshold.
- The <u>maximum length of shoreline contacted by oil</u> is determined by recording the maximum length of shoreline (measured as grid cells) contacted by oil above a specified threshold.
- The <u>probability of oil exposure to a receptor</u> is determined by recording the number of spill trajectories to reach a specified sea surface or subsea threshold within a receptor polygon, divided by the total number of spill trajectories within that scenario.
- The <u>minimum time before oil exposure to a receptor</u> is determined by ranking the elapsed time before sea surface exposure, at a specified threshold, to grid cells within a receptor polygon and recording the minimum value.
- The <u>probability of oil contact to a receptor</u> is determined by recording the number of spill trajectories to reach a specified shoreline contact threshold within a receptor polygon, divided by the total number of spill trajectories within that scenario.
- The <u>minimum time before shoreline contact to a receptor</u> is determined by ranking the elapsed time before shoreline contact, at a specified threshold, to grid cells within a receptor polygon and recording the minimum value.
- The <u>average potential oil loading within a receptor</u> is determined taking the average of the maximum loading to any grid cell within a polygon, for all simulations within a scenario/season, that recorded shoreline.
- The <u>maximum potential oil loading within a receptor</u> is determined by identifying the maximum loading to any grid cell within a receptor polygon, for a scenario.



- The <u>average volume of oil ashore within a receptor</u> is determined by calculating the average volume of oil to come ashore within a receptor polygon, from all the single spill trajectories which were predicted to make shoreline contact within a scenario.
- The <u>maximum volume of oil ashore within a receptor</u> is determined by recording the maximum volume of oil to come ashore within a receptor polygon, from all the single spill trajectories which were predicted to make shoreline contact within a scenario.
- The <u>average length of shoreline contacted within a receptor</u> is determined by calculating the average of the length of shoreline (measured as grid cells) contacted by oil within a receptor polygon, at a specified threshold, from all the single spill trajectories which were predicted to make shoreline contact within a scenario.
- The *maximum length of shoreline contacted by oil* is determined by recording the maximum length of shoreline (measured as grid cells) contacted by oil within a receptor polygon, at a specified threshold, from all the single spill trajectories which were predicted to make shoreline contact within a scenario.

8.2 Receptors Assessed

A range of environmental receptors and biological receptors and shorelines were assessed for sea surface exposure, shoreline contact and water column exposure as part of the study (see Table 12). The receptors are presented graphically in Figure 20 to Figure 34.

Note, the release location is situated within the Otway Integrated Marine and Coastal Regionalisation of Australia (IMCRA) receptor and hence this receptor will register all maximum values predicted by the modelling.

Receptor Category	Acronym	Hydrocarbon Exposure Assessment				
		Water Column	Sea Surface	Shoreline		
Marine National Park	MNP	~	~	×		
Australian Marine Park	AMP	~	~	×		
National Park	NP	~	~	×		
Integrated Marine and Coastal Regionalisation of Australia	IMCRA	~	~	×		
Interim Biogeographic Regionalisation of Australia	IBRA	~	~	~		
Key Ecological Feature	KEF	~	~	×		
Reefs, Shoals and Banks	RSB	~	~	×		
Ramsar	Ramsar	~	~	~		
State Waters	State Waters	~	~	×		
Local Government Areas	LGA	~	~	✓		

Table 12 Summary of receptors used to assess surface, shoreline and in-water exposure to hydrocarbons



Receptor Category	Acronym	Hydrocarbon Exposure Assessment				
		Water Column	Sea Surface	Shoreline		
Sub-Local Government Areas	Sub-LGA	\checkmark	\checkmark	\checkmark		



Figure 20 Receptor map for Marine National Parks.





Figure 21 Receptor map for Australian Marine Parks.









Figure 23 Receptor map illustrating the Integrated Marine and Coastal Regionalisation of Australia (IMCRA) receptors.



Figure 24 Map illustrating the Interim Biogeographic Regionalisation of Australia (IBRA) receptors.





Figure 25 Receptor map of Key Ecological Features (KEF)









Figure 27 Receptor map of RAMSAR sites









Figure 29 Receptor map of Local Government Areas (LGA) (2/3)









Figure 31 Receptor map of Sub-Local Government Areas (Sub-LGA) (1/3)



Figure 32 Receptor map of Sub-Local Government Areas (Sub-LGA) (2/3)





Figure 33 Receptor map of Sub-Local Government Areas (Sub-LGA) (3/3)



Figure 34 Receptor map of state waters.

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9 RESULTS: 300 M³ SURFACE RELEASE OF MARINE DIESEL OIL

The scenario examined a 300 m³ release of MDO over 6 hours (tracked for 30 days) to represent a containment loss from a vessel at the Artisan-1 well location. A total of 100 spill trajectories were simulated for each of the seasons assessed, summer and winter.

Section 9.1 presents stochastic results in tabulated format.

Note, no shoreline contact was predicted for any of the seasons modelled above the minimum threshold.

9.1 Stochastic Analysis

9.1.1 Sea Surface Exposure

Table 13 presents a summary of the maximum distances and directions travelled by oil on the sea surface at the low (0.5-10 g/m²), moderate (10-25 g/m²) and high (>25 g/m²) exposure thresholds for the two seasons. During summer conditions, low and moderate exposure was predicted up to 68 km and 12 km from the release location, respectively. Under winter conditions, low and moderate exposure was predicted up to 93 km and 10 km from the release location, respectively.

Table 14 presents the potential sea surface exposure to individual receptors predicted during summer and winter conditions. The modelling results demonstrated a 1% probability of oil exposure on the sea surface for the Central Victoria IMCRA receptor during the summer conditions. Stochastic results obtained during winter conditions exhibited a 1% probability of oil exposure on the sea surface for several receptors including the Central Victoria and Central Bass Strait IMCRA receptors, Apollo AMP and within Victorian State Waters.

None of the receptors were exposed at or above the moderate or high thresholds, with the exception of Otway IMCRA. Th Otway IMCRA receptor recorded low, moderate and high exposure due to the release location being situated within the boundaries of this receptor.

Season	Distance and direction	exposure				
		Low	Moderate	High		
	Max. distance from release location (km)	68	12	6		
Summer	Max distance from release location (km) (99 th percentile)	35	11	6		
	Direction	E	NNE	E		
	Max. distance from release location (km)	93	10	6		
Winter	Max distance from release location (km) (99 th percentile)	56	10	6		
	Direction	E	WNW	ENE		

Table 13Maximum distance and direction travelled on the sea surface by a single spill trajectory
from the release location to the specified oil exposure thresholds.



Table 14 Summary of the potential sea surface exposure to individual receptors

			surfa	surface (hours) for each threshold				
Season	Receptor		Low	Moderate	High	Low	Moderate	High
Summer		Otway	100	98	48	1	1	1
	IMCRA	Central Victoria	1	-	-	89	-	-
		Otway	100	98	41	1	1	1
	IMCRA	Central Victoria	1	-	-	133	-	-
Winter		Central Bass Strait	1	-	-	71	-	-
	AMP	Apollo	1	-	-	35	-	-
	State Waters Victoria State Waters		1	-	-	133	-	-

Probability of oil exposure on the sea surface (%) for each threshold Minimum time before oil exposure on the sea

9.1.2 Water Column Exposure

9.1.2.1 **Dissolved Hydrocarbons**

Table 15 and Table 16 summarise the probability and maximum dissolved hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual receptors in the 0-10 m depth layer, during summer and winter conditions.

The averaged dissolved hydrocarbon concentrations over 48 hours was highest within the Otway IMCRA receptor which registered 8 ppb and 9 ppb during summer and winter conditions, respectively. A 1% probability of exposure. No other receptors were exposed at or above the specified thresholds.

Based on the 1 hour exposure window, the Otway IMCRA receptor recorded the greatest dissolved hydrocarbon concentration of 76 ppb during summer and 59 ppb during winter. The Otway IMCRA receptor recorded a probability of 2% and 3% during the summer and winter conditions, respectively, based on the moderate threshold. There was no predicted exposure to other receptors at the moderate or high thresholds.

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Table 15Predicted probability and maximum dissolved hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer, during summer conditions.

SUMMER Receptor		Maximum dissolvedProbability of time-averaged dissolved hydrocarbon exposure for 48 hour window		Maximum dissolved hydrocarbon	Probability of instantaneous dissolved hydrocarbon exposure for 1 hour window				
		exposure (ppb) for 48 hour window	Low	Moderate	High	exposure (ppb) for 1 hour window	Low	Moderate	High
LGA	Colac Otway	1	-	-	-	6	1	-	-
SUB-LGA	Apollo Bay	1	-	-	-	6	1	-	-
	Otway	8	1	-	-	76	47	2	-
IMCRA	Central Victoria	1	-	-	-	21	2	-	-
	Central Bass Strait	1	-	-	-	20	1	-	-
	Otway Ranges	1	-	-	-	6	1	-	-
IBRA	Otway Plain	1	-	-	-	5	-	-	-
AMP	Apollo	1	-	-	-	22	3	-	-
State Waters	Victoria State Waters	1	-	-	-	17	2	-	-

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Table 16Predicted probability and maximum dissolved hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer, during winter conditions.

WINTER Receptor		Maximum dissolved hydrocarbon	Maximum dissolvedProbability of time-averaged dissolved hydrocarbon exposure*N		Maximum dissolved hydrocarbon exposure (ppb) for 1	Probability of instantaneous dissolved hydrocarbon exposure for 1 hour window			
		exposure (ppb) for 48 hour window	Low	Moderate	High	hour window	Low	Moderat e	High
LGA	Colac Otway	1	-	-	-	8	1	-	-
SUB-LGA	Cape Otway West	1	-	-	-	8	1	-	-
	Otway	9	2	-	-	59	70	3	-
IMCRA	Central Victoria	2	-	-	-	19	3	-	-
	Central Bass Strait	1	-	-	-	17	2	-	-
	Otway Ranges	1	-	-	-	5	-	-	-
IBRA	Otway Plain	1	-	-	-	8	1	-	-
AMP	Apollo	2	-	-	-	24	5	-	-
State Waters	Victoria State Waters	1	-	-	-	13	2	-	-



9.1.2.2 Entrained Hydrocarbons

Table 17 and Table 18 summarise the probability and maximum entrained hydrocarbon exposure for 1 hour and 48-hour exposure windows) to individual receptors in the 0–10 m depth layer, during summer and winter conditions.

The maximum entrained hydrocarbon concentrations over 48 hour exposure window during summer and winter conditions was 2,182 ppb and 792 ppb, respectively. None of the receptors with the exception of the Otway IMCRA receptor were exposed at or above the moderate (100-1,000 ppb) or high (>1,000 ppb) thresholds during summer or winter conditions.

Based on the 1 hour exposure window, the maximum entrained hydrocarbon concentrations predicted for the Otway IMCRA receptor during summer and winter conditions was 5,933 ppb and 5,046 ppb, respectively. The probability of exposure at or above the moderate (100-1,000 ppb) threshold to receptors other than IMCRA Otway (83% summer and 93% winter) ranged from 1% (Cape Patton sub-LGA) to 8% (Victorian State Waters) during summer conditions and 1% (Twelve Apostles MNP) to 16% (Apollo AMP) during winter conditions. None of the receptors was exposed at or above the high threshold (1,000 ppb), with the exception of IMCRA – Otway.

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Table 17Predicted probability and maximum entrained hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer during summer conditions.

SUMMER		Maximum time- entrained hydrocarbon	Proba hydroca	Probability of entrained Ma hydrocarbon exposure for 48 hour window exp		Maximum entrained hydrocarbon exposure (ppb) for 1	Probability of entrained hydrocarbon exposure for 1 hour window		
Receptor		48 hour window	Low	Moderat e	High	nour window	Low	Moderat e	High
AMP	Apollo	166	_	-	-	406	25	7	-
	Glenelg Plain	58	-	-	-	33	9	-	-
	Bridgewater	58		-	-	31	5	-	-
	Warrnambool Plain	317	-	-	-	228	25	4	-
IBRA	Otway Ranges	254	-	-	-	218	25	2	-
	Otway Plain	284	-	-	-	208	28	3	-
	Gippsland Plain	39	-	-	-	21	1	-	-
	Wilsons Promontory	21	-	-	-	12	1	-	-
	Otway	2,182	1	-	-	5,933	97	83	39
	Victorian Embayments	14	-	-	-	11	1	-	-
IMCRA	Central Victoria	178	-	-	-	399	22	5	-
	Central Bass Strait	172	-	-	-	334	13	2	-
	Flinders	22	-	-	-	13	1	-	-
KEF	Bonney Coast Upwelling	125	-	-	-	98	22	-	-
	Discovery Bay	48	-	-	-	25	3	-	-
MINP	Twelve Apostles	372	-	-	-	278	26	6	-
	Lower South East	24	-	-	-	22	2	-	-
NP	Bunurong Marine Park	24	-	-	-	14	1	-	-
	Wilsons Promontory Marine Park	21	-	-	-	12	1	-	-
	Phillip Island	20	-	-	-	19	1	-	-
LGA	Norman Island	21	-	-	-	12	1	-	-

	Shellback Island	20	-	-	-	11	1	-	-
	Glenelg	58	-	-	-	33	9	-	-
	Warrnambool	46	-	-	-	24	8	-	-
	Moyne	172	-	-	-	96	17	-	-
	Corangamite	317	-	-	-	218	26	4	-
	Colac Otway	284	-	-	-	208	28	3	-
	Surf Coast	69	-	-	-	48	5	-	-
	Mornington Peninsula	19	-	-	-	11	1	-	-
	Bass Coast	40	-	-	-	21	1	-	-
	South Gippsland	22	-	-	-	12	1	-	-
	Grant	26	-	-	-	20	1	-	-
	Lady Julia Percy Island	73	-	-	-	43	5	-	-
	Laurence Rocks	41	-	-	-	26	7	-	-
State	South Australia State Waters	31	-	-	-	26	2	-	-
Waters	Victoria State Waters	372	-	-	-	388	30	8	-
	Wilsons Promontory (West)	22	-	-	-	12	1	-	-
	Venus Bay	21	-	-	-	13	1	-	-
	Kilcunda	40	-	-	-	21	1	-	-
	French Island / San Remo	14	-	-	_	10	1	-	-
	Mornington Peninsula (SW)	18	-	-	-	10	1	-	-
	Port Phillip (Sorrento Shore)	18	-	-	-	11	1	-	-
SUB-LGA	Anglesea	21	-	-	_	13	3	-	-
	Lorne	78	-	-	_	49	5	-	-
	Cape Patton	156	-	-	-	132	14	1	-
	Apollo Bay	168	-	-	-	208	21	3	-
	Cape Otway West	284	-	-	-	197	28	2	-
	Moonlight Head	317	-	-	-	218	26	4	-
H	Port Campbell	220	-	-	-	157	18	2	-

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Bay of Islands	172	-	-	-	96	17	-	-
Childers Cove	62	-	-	-	43	10	-	-
Warrnambool	27	-	-	-	23	7	-	-
Port Fairy	56	-	-	-	36	2	-	-
Portland Bay (East)	31	-	-	-	21	2	-	-
Portland Bay (West)	38	-	-	-	21	1	-	-
Cape Nelson	58	-	-	-	31	9	-	-
Discovery Bay (East)	46	-	-	-	24	2	-	-
Discovery Bay (West)	24	-	-	-	16	2	-	-

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Table 18Predicted probability and maximum entrained hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer during winter conditions.

WINTER		Maximum time- entrained hydrocarbon	Proba hydroca	ability of ent rbon exposi hour windov	rained ure for 48 w	Maximum entrained hydrocarbon exposure (ppb) for 1	Probability of entrained hydrocarbon exposure for 1 hour window			
Receptor		48 hour window	Low	Low Moderat e		nour window	Low	Moderate	High	
	Apollo	99	-	-	-	501	54	16	-	
	Beagle	6	-	-	-	11	2	-	-	
	Flinders	5	-	-	-	10	1	-	-	
	Warrnambool Plain	54	-	-	-	98	17	-	-	
IBRA	Otway Ranges	169	-	-	-	196	21	4	-	
	Otway Plain	298	-	-	-	448	27	6	-	
	Gippsland Plain	20	-	-	-	23	8	-	-	
	Strzelecki Ranges	12	-	-	-	13	1	-	-	
	Wilsons Promontory	19	-	-	-	21	3	-	-	
	Twofold Shelf	5	-	-	-	10	1	-	-	
	Otway	792	2	-	-	5,046	99	93	58	
	Victorian Embayments	18	-	-	-	20	3	-	-	
INCRA	Central Victoria	137	-	-	-	446	54	14	-	
	Central Bass Strait	69	-	-	-	386	51	13	-	
	Flinders	19	-	-	-	22	4	-	-	
VEE	West Tasmania Canyons	12	-	-	-	14	1	-	-	
NEF	Bonney Coast Upwelling	13	-	-	-	15	1	-	-	
	Bunurong	10	-	-	-	12	1	-	-	
MNP	Point Addis	16	-	-	-	17	2	-	-	
	Port Phillip Heads	15	-	-	-	19	4	-	-	

	Twelve Apostles	129	-	-	-	283	15	1	-
	Wilsons Promontory	14	-	-	-	16	3	-	-
NP	Wilsons Promontory Marine Park	17	-	-	-	20	2	-	-
RAMSAR	Port Phillip Bay and Bellarine Peninsula	7	-	-	-	10	1	-	-
	Phillip Island	19			22	3	-	-	
	Hogan Island Group	5	-	-	-	10	1	-	-
	Glennie Group	14	-	-	-	15	3	-	-
	Norman Island	19	-	-	-	20	3	-	-
	Shellback Island	17	-	-	-	21	2	-	-
	Anser Island	11	-	-	-	12	2	-	-
	Kanowna Island	10	-	-	-	12	2	-	-
	Skull Rock	10	-	-	-	12	2	-	-
LGA	Warrnambool	8	-	-	-	10	1	-	-
	Moyne	49	-	-	-	71	6	-	-
	Corangamite	44	-	-	-	98	18	-	-
	Colac Otway	298	-	-	-	448	27	6	-
	Surf Coast	21	-	-	-	23	3	-	-
	Greater Geelong	20	-	-	-	22	3	-	-
	Mornington Peninsula	20	-	-	-	23	8	-	-
	South Gippsland	18	-	-	-	21	2	-	-
	Lady Julia Percy Island	8	-	-	-	11	1	-	-
State	Tasmania State Waters	6	-	-	-	11	2	-	-
Waters	Victoria State Waters	298	-	-	-	548	40	9	-
	Wilsons Promontory (West)	18	-	-	-	21	2	-	-
SUB-LGA	Waratah Bay	12	-	-	-	13	1	-	-
	Cape Liptrap (NW)	13	-	-	-	15	1	-	-

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Westernport	11	-	-	-	14	2	-	-
Mornington Peninsula (S)	14	-	-	-	16	8	-	-
Mornington Peninsula (SW)	20	-	-	-	23	8	-	-
Port Phillip (Sorrento Shore)	20	-	-	-	22	4	-	-
Port Phillip Heads	10	-	-	-	13	3	-	-
Port Phillip (Queenscliff)	11	-	-	-	15	3	-	-
Torquay	20	-	-	-	22	2	-	-
Anglesea	12	-	-	-	14	2	-	-
Lorne	16	-	-	-	18	3	-	-
Cape Patton	68	-	-	-	95	7	-	-
Apollo Bay	70	-	-	-	84	27	-	-
Cape Otway West	298	-	-	-	448	27	6	-
Moonlight Head	44	-	-	-	98	18	-	-
Port Campbell	43	-	-	-	65	7	-	-
Bay of Islands	49	-	-	-	71	6	-	-
Childers Cove	31	-	-	-	41	1	-	-

*Concentration recorded over a 48-hour window.

RPS

^Instantaneous concentration recorded over one hour.

10 RESULTS: 222,224 BBL SUBSEA RELEASE OF CONDENSATE

The scenario examined a 222,224 bbl subsea release of Thylacine condensate over 86 days (tracked for 114 days) to represent an unrestricted open-hole loss of well control from Artisan-1 well location. A total of 100 spill trajectories were simulated for each of the seasons assessed, summer and winter.

Section 10.1 presents stochastic results for sea surface, shoreline and in-water exposure in tabulated format.

10.1 Stochastic Analysis

10.1.1 Sea Surface Exposure and Shoreline Contact

Table 19 presents a summary of the maximum distance and direction travelled by condensate on the sea surface at the low (0.5-10 g/m²), moderate (10-25 g/m²) and high (>25 g/m²) exposure thresholds for each of the two seasons considered, summer and winter. During summer conditions, low and moderate exposure of surface hydrocarbons were predicted up to 52 km and 4 km from the release location, respectively, while during winter, low and moderate exposure surface hydrocarbons extended to a maximum distance of 53 km and 3 km from the release location, respectively. Note, no high exposure from surface hydrocarbons was predicted for any of the seasons assessed.

Table 20 presents the potential sea surface exposure to individual receptors predicted during summer and winter conditions. The probability of hydrocarbon exposure on the sea surface at or above the low threshold was predicted to range from 6% (Otway Ranges IBRA) to 16% (Colac Otway LGA, Cape Otway West sub-LGA and Victorian State Waters) during summer conditions, with the exception of Otway IMCRA receptor (100%). The winter stochastic modelling results demonstrated a larger number of receptors potentially exposed to surface hydrocarbons at or above low levels with a probability of exposure predicted to range from 3% (Twelve Apostles MNP and Otway Ranges IBRA) to 40% (Otway Plain IBRA, Cape Otway West sub-LGA and Colac Otway LGA), with the exception of Otway IMCRA (100%) and within Victorian State Waters (57%). None of the receptors other than the Otway IMCRA were exposed at or above the moderate or high thresholds for any seasons assessed.

Table 21 presents a summary of potential hydrocarbon contact to any shorelines for summer and winter conditions while Table 22 summarises potential shoreline contact to individual receptors, for each season.

The probability of contact to any shoreline was 16% and 57% for the summer and winter season, respectively, while the minimum time for visible surface hydrocarbon to reach a shoreline was 3 days for 5 days, respectively. The maximum volume of hydrocarbons predicted to come ashore was 15 m³ and 33 m³, during summer and winter conditions, respectively, while the maximum length of shoreline contacted above the low threshold (>10 g/m²) was 7.0 km and 11.0 km, respectively. Note, no shoreline loading above 1,000 g/m² was predicted.

The Otway IMCRA shoreline was the only receptor to record of contact above 100 g/m² with a probability of 3% during summer and 2% during winter conditions. The modelling results during winter conditions demonstrated additional shoreline contact to Moyne, Corangamite, Moonlight head and Childers Cove.

Table 19Maximum distance and direction travelled on the sea surface by a single spill trajectory
from the release location to the specified oil exposure thresholds.

Soason	Distance and direction	Zones of p	Zones of potential sea surface exposure						
Season	Distance and direction	Low	Moderate	High					
	Max. distance from release site (km)	52	4	NA					
Summer I	Max distance from release site (km) (99 th percentile)	34	4	NA					
	Direction	E	E	NA					
	Max. distance from release site (km)	53	3	NA					
Winter	Max distance from release site (km) (99 th percentile)	49	3	NA					
	Direction	NNW	W	NA					

Table 20 Summary of the potential sea surface exposure to individual receptors

			Probabili the	ty of oil expo sea surface (osure on (%)	Minimum time before oil exposure on the sea surface (hours)			
Season		Receptor	Low	Moderate	High	Low	Moderate	High	
	LGA	Colac Otway	16	-	-	80	-	-	
	SUB-LGA	Cape Otway West	16	-	-	80	-	-	
Summer	IMCRA	Otway	100	100	-	1	3	-	
Summer	IBRA	Otway Ranges	6	-	-	1,343	-	-	
	IDKA	Otway Plain	12	-	-	80	-	-	
	State Waters	Victoria State Waters	16	-	-	80	-	-	
	LGA	Moyne	8	-	-	649	-	-	
		Corangamite	14	-	-	311	-	-	
		Colac Otway	40	-	-	188	-	-	
		Cape Otway West	40	-	-	188	-	-	
	SUB-LGA	Moonlight Head	14	-	-	311	-	-	
\\/;inter		Childers Cove	8	-	-	649	-	-	
winter	IMCRA	Otway	100	100	-	1	2	-	
		Warrnambool Plain	22	-	-	311	-	-	
	IBRA	Otway Ranges	3	-	-	413	-	-	
		Otway Plain	40	-	-	188	-	-	
	MNP	Twelve Apostles	3	-	-	821	-	-	
	State Waters	Victoria State Waters	57	-	-	188	-	-	



Shoreline statistics	Summer	Winter
Probability of contact to any shoreline (%)	16	57
Minimum time for visible oil to reach a shoreline (days)	3	5
Maximum volume of hydrocarbons ashore (m ³)	15	33
Average volume of hydrocarbons ashore (m ³)	1	5
Maximum length of the shoreline >10 g/m² (km)	7.0	11.0
Average shoreline length (km) >10 g/m ² (km)	4.7	5.6
Maximum length of the shoreline >100 g/m ² (km)	4.0	8.0
Average shoreline length (km) >100 g/m ² (km)	2.4	3.5
Maximum length of the shoreline >1,000 g/m ² (km)	-	-
Average shoreline length (km) > 1,000 g/m ² (km)	-	-

Table 21 Summary of potential oil contact to any shoreline for each season assessed

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		Probat	oility of sh oading (%	oreline	Minimu s accum	um time shorelin ulation	before e (hours)	Loa sho (g	ad on reline /m²)	Volui shor (n	me on reline n³)	Mea shore	Mean length of Maximum oreline contacted shoreline (km) (num len line con (km)	Im length of te contacted (km)	
Season	Receptor	>10 g/m²	>100 g/m²	>1,000 g/m²	>10 g/m²	>100 g/m²	>1,000 g/m²	Mea n	Peak	Mea n	Peak	>10 g/m²	>100 g/m²	>1,000 g/m²	>10 g/m²	>100 g/m²	>1,00 0 g/m²
	Colac Otway	16	15	-	77	277	-	136	520	1	15	5	2	-	7	4	-
Summer	Cape Otway West	16	15	-	77	277	-	136	520	1	15	5	2	-	7	4	-
	Moyne	8	8	-	26	27	-	88	130	<1	5	4	2	-	5	2	-
	Corangamite	14	10	-	635	654	-	241	984	2	23	4	3	-	5	3	-
	Colac Otway	40	40	-	125	247	-	194	670	5	33	6	4	-	11	8	-
Winter	Cape Otway West	40	40	-	109	174	-	194	670	5	33	6	4	-	11	8	-
	Moonlight Head	14	10	-	109	174	-	241	984	2	23	4	3	-	5	3	-
	Childers Cove	8	8	-	125	247	-	88	130	<1	5	4	2	-	5	2	-

Table 22 Summary of the potential shoreline contact to individual receptors for each season assessed


10.1.2 Water Column Exposure

10.1.2.1 Dissolved Hydrocarbons

Table 23 and Table 24 summarise the probability and maximum dissolved hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual receptors in the 0–10 m depth layer, during summer and winter conditions.

For the 48 hour time-averaged exposure window, dissolved hydrocarbons remained below 30 ppb in summer and 34 ppb in winter conditions, and hence no moderate or high exposure was predicted under the seasonal conditions modelled. During summer conditions, the probability of low exposure ranged from 1% (Bonney Coast Upwelling KEF, Moyne LGA, Bay of Islands and Childers Cove sub-LGAs) to 17% (Otway Plain IBRA, Colac Otway LGA, Cape Otway West sub-LGA and within Victoria State Waters)The Otway IMCRA recorded a probability of 50% during summer. During winter conditions, the probability of low exposure to dissolved hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF, Bay of Islands and Lorne sub-LGA) to 16% (within Victoria State Waters). The Otway IMCRA registered a probability of 42% for winter. None of the receptors were exposed to moderate (50 – 400 ppb) or high (>400 ppb) dissolved hydrocarbons (over a 48 hour basis) during the summer or winter season.

The analysis for the dissolved hydrocarbons over a 1 hour window showed that the maximum exposure was 309 ppb during summer and 289 ppb during winter, which was predicted within the Otway IMCRA and Victorian State Waters. During summer conditions, the probability of moderate exposure to dissolved hydrocarbons ranged from 1% (Glenelg Plain and Bridgewater IBRA's; Glenelg, Moyne and Surf Coast LGAs; Lorne, Bay of Islands, Childers Cove and Cape Nelson sub-LGAs) to 43% (Otway Plain IBRA, Colac Otway LGA, Cape Otway West sub-LGA and within Victoria State Waters). The probability for Otway IMCRA was 58%. Under winter conditions, the probability of moderate exposure (over 1 hour) to dissolved hydrocarbons ranged from 1% (Gippsland Plain IBRA; Flinders IMCRA; Point Addis and Wilsons Promontory MNP; Mornington Peninsula LGA; Lorne, Mornington Peninsula and Childers Cove sub-LGAs) to 57% for the Victorian State Waters. The probability of exposure to the Otway IMCRA was 68%. None of the receptors were exposed high concentrations during the summer or winter season.



Table 23Predicted probability and maximum dissolved hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer, during summer conditions.

SUMMER	SUMMER		Probabi disso exposure	lity of time lved hydro e for 48 ho	-averaged ocarbon ur window	Maximum dissolved hydrocarbon	Probability of instantaneous dissolved hydrocarbon exposure for 1 hour window		
Receptor		for 48 hour window	Low	Modera te	High	exposure (ppb) for 1 hour window	Low	Moderat e	High
	Apollo	20	11	-	-	225	98	30	-
	Beagle	1	-	-	-	9	1	-	-
AIVIE	Nelson	1	-	-	-	18	3	-	-
	Zeehan	1	-	-	-	19	4	-	-
	Glenelg Plain	6	-	-	-	53	25	1	-
	Bridgewater	4	-	-	-	54	20	1	-
	Warrnambool Plain	24	5	-	-	217	99	14	-
IBRA	Otway Ranges	13	7	-	-	161	100	27	-
	Otway Plain	23	17	-	-	235	98	43	-
	Gippsland Plain	3	-	-	-	28	11	-	-
	Wilsons Promontory	1	-	-	-	12	3	-	-
	Coorong	0	-	-	-	12	1	-	-
	Otway	30	50	-	-	309	100	58	-
	Victorian Embayment	3	-	-	-	31	6	-	-
INICRA	Central Victoria	18	9	-	-	253	95	28	-
	Central Bass Strait	17	6	-	-	254	88	20	-
	Flinders	2	-	-	-	26	5	-	-
VEE	West Tasmania Canyons	2	-	-	-	34	8	-	-
NEF	Bonney Coast Upwelling	10	1	-	-	97	60	2	-
	Churchill Island	1	-	-	-	7	2	-	-
	Discovery Bay	3	-	-	-	41	15	-	-
	Point Addis	2	-	-	-	34	14	-	-
IVIINP	Port Phillip Heads	2	-	-	-	21	7	-	-
	Twelve Apostles	27	6	-	-	217	98	20	-
	Wilsons Promontory	2	-	-	-	12	2	-	-

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MD	Lower South East	1	-	-	-	16	3	-	-
	Bunurong Marine Park	1	-	-	-	10	3	-	-
ND	Wilsons Promontory Marine Park	1	-	-	-	6	1	-	-
INF	Port Phillip Bay and Bellarine Peninsula	1	-	-	-	31	4	-	-
RAMSAR	Western Port	1	-	-	-	12	2	-	-
	Phillip Island	2	-	-	-	24	11	-	-
	Mud Island	1	-	-	-	12	2	-	-
	Moncoeur Islands	1	-	-	-	9	1	-	-
	Rodondo Island	1	-	-	-	11	2	-	-
	Glennie Group	1	-	-	-	12	3	-	-
	Norman Island	1	-	-	-	10	1	-	-
	Anser Island	1	-	-	-	6	1	-	-
	Kanowna Island	1	-	-	-	10	1	-	-
SHORE	Skull Rock	1	-	-	-	7	1	-	-
	Glenelg	6	-	-	-	54	25	1	-
	Warrnambool	5	-	-	-	46	25	-	-
	Moyne	7	1	-	-	66	74	1	-
	Corangamite	24	5	-	-	217	100	17	-
	Colac Otway	23	17	-	-	235	100	43	-
	Surf Coast	5	-	-	-	57	24	1	-
	Greater Geelong	2	-	-	-	31	8	-	-
	Mornington Peninsula	3	-	-	-	28	11	-	-
	Bass Coast	1	-	-	-	21	5	-	-
	South Gippsland	1	-	-	-	7	1	-	-
	Grant	1	-	-	-	19	3	-	-
	Lady Julia Percy Island	2	-	-	-	28	22	-	-
	Laurence Rocks	5	-	-	-	18	20	-	-
State	South Australia State Waters	1	-	-	-	26	6	-	-
Waters	Victoria State Waters	30	17	-	-	309	100	43	-
	Wilsons Promontory (West)	1	-	-	-	6	1	-	-
SUB-LGA	Cape Liptrap (NW)	1	-	-	-	7	1	-	-
	Venus Bay	1	-	-	-	10	3	-	-

Kilcunda	1	-	-	-	21	5	-	-
French Island / San Remo	1	-	-	-	14	4	-	-
French Island / Crib Point	1	-	-	-	6	1	-	-
Westernport	1	-	-	-	13	6	-	-
Mornington Peninsula (S)	1	-	-	-	14	7	-	-
Mornington Peninsula (SW)	2	-	-	-	24	11	-	-
Port Phillip (Sorrento Shore)	3	-	-	-	23	8	-	-
Port Phillip Heads	1	-	-	-	31	6	-	-
Port Phillip (Queenscliff)	2	-	-	-	23	7	-	-
Torquay	3	-	-	-	23	8	-	-
Anglesea	3	-	-	-	32	12	-	-
Lorne	5	-	-	-	57	24	1	-
Cape Patton	11	2	-	-	161	85	8	-
Apollo Bay	13	4	-	-	154	95	15	-
Cape Otway West	23	17	-	-	235	100	43	-
Moonlight Head	24	5	-	-	217	100	17	-
Port Campbell	12	3	-	-	103	77	6	-
Bay of Islands	7	1	-	-	66	74	1	-
Childers Cove	7	1	-	-	55	55	1	-
Warrnambool	3	-	-	-	36	16	-	-
Port Fairy	2	-	-	-	23	11	-	-
Portland Bay (East)	1	-	-	-	10	2	-	-
Cape Nelson	6	-	-	-	54	25	1	-
Discovery Bay (East)	1	-	-	-	11	2	-	-
Discovery Bay (West)	1	-	-	-	8	1	-	-



Table 24Predicted probability and maximum dissolved hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer, during winter conditions .

WINTER		Maximum dissolved hydrocarbon	Probabi disso exposure	lity of time- lved hydro e for 48 hou	averaged carbon ur window	Maximum dissolved hydrocarbon exposure (ppb) for 1	Probability of instantaneous dissolved hydrocarbon exposure for 1 hour window			
Receptor		exposure (ppb) for 48 hour window	Low	Modera te	High	nour window	Low	Moderat e	High	
	Apollo	13	7	-	-	237	100	39	-	
AMP	Beagle	2	-	-	-	37	13	-	-	
	Zeehan	1	-	-	-	16	3	-	-	
	King Island	1	-	-	-	9	1	-	-	
	Flinders	1	-	-	-	9	2	-	-	
	Glenelg Plain	4	-	-	-	19	2	-	-	
	Bridgewater	2	-	-	-	8	1	-	-	
	Warrnambool Plain	14	4	-	-	237	100	21	-	
IBRA	Otway Ranges	14	6	-	-	248	100	35	-	
	Otway Plain	30	10	-	-	203	100	51	-	
	Gippsland Plain	6	-	-	-	51	16	1	-	
	Strzelecki Ranges	4	-	-	-	31	18	-	-	
	Wilsons Promontory	4	-	-	-	34	21	-	-	
	Twofold Shelf	2	-	-	-	28	6	-	-	
	Otway	34	42	-	-	289	100	68	-	
	Victorian Embayments	4	-	-	-	36	9	-	-	
IMCRA	Central Victoria	25	7	-	-	235	100	33	-	
	Central Bass Strait	17	4	-	-	282	100	26	-	
	Flinders	5	-	-	-	66	27	1	-	
	West Tasmania Canyons	4	-	-	-	36	8	-	-	
KEF	Bonney Coast Upwelling	6	1	-	-	86	19	2	-	
	Upwelling East of Eden	1	-	-	-	9	1	-	-	
	Bunurong	2	-	-	-	34	10	-	-	
MNP	Churchill Island	1	-	-	-	8	1	-	-	
	Point Addis	5	-	-	-	51	41	1	-	

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	Port Phillip Heads	1	-	-	-	15	8	-	-
	Twelve Apostles	16	6	-	-	155	100	18	-
	Wilsons Promontory	5	-	-	-	66	23	1	-
	Bunurong Marine Park	1	-	-	-	24	8	-	-
NP	Wilsons Promontory Marine Park	4	-	-	-	33	9	-	-
RAMSAR	Port Phillip Bay and Bellarine Peninsula	1	-	-	-	14	2	-	-
	Western Port	3	-	-	-	22	2	-	-
	King Island	1	-	-	-	9	1	-	-
	Seal Islands	2	-	-	-	15	2	-	-
	Phillip Island	3	-	-	-	26	13	-	-
	French Island	1	-	-	-	10	1	-	-
	Moncoeur Islands	1	-	-	-	26	8	-	-
	Hogan Island Group	1	-	-	-	9	2	-	-
	Rodondo Island	1	-	-	-	24	13	-	-
	Glennie Group	4	-	-	-	34	21	-	-
	Norman Island	3	-	-	-	33	16	-	-
	Shellback Island	2	-	-	-	24	9	-	-
	Anser Island	2	-	-	-	27	18	-	-
011005	Kanowna Island	3	-	-	-	18	18	-	-
SHORE	Skull Rock	3	-	-	-	16	18	-	-
	Glenelg	4	-	-	-	19	2	-	-
	Warrnambool	5	-	-	-	34	13	-	-
	Moyne	14	4	-	-	87	60	5	-
	Corangamite	14	5	-	-	237	100	21	-
	Colac Otway	30	10	-	-	212	100	51	-
	Surf Coast	4	-	-	-	46	50	-	-
	Greater Geelong	2	-	-	-	26	15	-	-
	Mornington Peninsula	6	-	-	-	52	13	1	-
	Bass Coast	2	-	-	-	24	9	-	-
	South Gippsland	4	-	-	-	43	18	-	-
	Lady Julia Percy Island	2	-	-	-	20	7	-	-

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	Laurence Rocks	1	-	-	-	19	2	-	-
State	Tasmania State Waters	1	-	-	-	15	3	-	-
Waters	Victoria State Waters	34	16	-	-	289	100	57	-
	Wilsons Promontory (East)	2	-	-	-	31	11	-	-
	Wilsons Promontory (West)	4	-	-	-	33	14	-	-
	Waratah Bay	4	-	-	-	31	18	-	-
	Cape Liptrap (NW)	4	-	-	-	43	16	-	-
	Venus Bay	2	-	-	-	24	9	-	-
	Kilcunda	1	-	-	-	18	7	-	-
	French Island / San Remo	1	-	-	-	8	2	-	-
	French Island / Crib Point	1	-	-	-	8	1	-	-
	Westernport	6	-	-	-	31	6	-	-
	Mornington Peninsula (S)	6	-	-	-	51	12	1	-
	Mornington Peninsula (SW)	4	-	-	-	33	11	-	-
	Port Phillip (Sorrento Shore)	2	-	-	-	26	10	-	-
	Port Phillip Heads	1	-	-	-	14	4	-	-
	Port Phillip (Queenscliff)	2	-	-	-	25	15	-	-
SUD-LGA	Torquay	3	-	-	-	44	16	-	-
	Anglesea	4	-	-	-	40	31	-	-
	Lorne	7	1	-	-	57	50	1	-
	Cape Patton	13	3	-	-	124	92	8	-
	Apollo Bay	14	4	-	-	212	100	21	-
	Cape Otway West	30	10	-	-	203	100	51	-
	Moonlight Head	14	4	-	-	237	100	21	-
	Port Campbell	9	3	-	-	112	67	5	-
	Bay of Islands	14	1	-	-	90	60	5	-
	Childers Cove	14	4	-	-	78	24	1	-
	Warrnambool	1	-	-	-	9	3	-	-
	Port Fairy	5	-	-	-	29	3	-	-
	Portland Bay (East)	1	-	-	-	15	1	-	-
	Cape Nelson	4	-	-	-	19	2	-	-

*Concentration recorded over a 48-hour window. ^Instantaneous concentration recorded over one hour. •



10.1.2.2 Entrained Hydrocarbons

Table 25 and Table 26 summarise the probability and maximum entrained hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual receptors in the 0–10 m depth layer at, or above the exposure thresholds during summer and winter.

The maximum entrained hydrocarbon exposure over 48 hour window predicted for the summer and winter season was 559 ppb and 569 ppb, respectively, and hence no moderate or high exposure was predicted. During summer conditions, the probability of low exposure to entrained hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF; Moyne LGA; Bay of Islands and Childers Cove sub-LGAs) to 17% (Otway Plain IBRA; Colac Otway LGA; Cape Otway West sub-LGA and within Victorian State Waters), with the exception of IMCRA – Otway (50%). During winter conditions, the probability of low exposure to entrained hydrocarbons over 48 hours ranged from 1% (Bonney Coast Upwelling KEF; Bay of Islands and Lorne sub-LGAs) to 16% (Victoria State Waters), with the exception of Otway IMCRA (42%).

For the 1 hour exposure window, the entrained hydrocarbon concentrations had peaked at 948 ppb during summer and 932 ppb during winter with the maximum values predicted within the Otway IMCRA During summer conditions, the probability of moderate entrained hydrocarbon exposure ranged from 7% (Cape Patton sub-LGA) to 73% (Victorian State Waters). The probability of exposure to the Otway IMCRA receptor was 100% during both seasons. For other receptors during winter conditions, the probability of moderate entrained hydrocarbon exposure to the Otway IMCRA receptor was 100% during both seasons. For other receptors during winter conditions, the probability of moderate entrained hydrocarbon exposure ranged from 8% (along the shoreline of Childers Cove sub-LGA; Moyne and Warrnambool LGA) to 73% (within Victorian State Waters).



Table 25Predicted probability and maximum entrained hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual
receptors in the 0–10 m depth layer during summer conditions.

Receptor		Maximum time- entrained hydrocarbon	Proba hydroca	bility of ent rbon exposu hour windov	rained ure for 48 v	Maximum entrained hydrocarbon exposure (ppb) for 1 bour window	Probability of entrained hydrocarbon exposure for 1 hour window			
-		48 hour window	Low	Moderat e	High		Low	Moderate	High	
	Apollo	81	11	-	-	255	98	50	-	
AMP	Beagle	12		-	-	15	14		-	
	Murray	7		-	-	10	1	-	-	
	Zeehan	7		-	-	14	8		-	
	Glenelg Plain	36	-	-	-	41	45		-	
	Bridgewater	32		-	-	37	36		-	
	Warrnambool Plain	255	5	-	-	293	100	38	-	
IBRA	Otway Ranges	184	7	-	-	215	100	29	-	
	Otway Plain	294	17	-	-	333	100	71	-	
	Gippsland Plain	41		-	-	47	62	-	-	
	Strzelecki Ranges	18		-	-	20	14	-	-	
	Wilsons Promontory	24	-	-	-	28	21	-	-	
	Coorong	9		-	-	13	12	-	-	
	Otway	559	50	-	-	948	100	100	-	
IMCRA	Victorian Embayment	37		-	-	42	52		-	
	Central Victoria	117	9	-	-	255	96	50	-	
	Central Bass Strait	94	6	-	-	220	95	38	-	
	Flinders	24		-	-	28	29		-	
KEE	West Tasmania Canyons	16		-	-	25	16	-	-	
·····	Bonney Coast Upwelling	36	1	-	-	53	74		-	
	Bunurong	12	_	-	-	14	19	-	-	
	Churchill Island	11		-	-	13	12	-	-	
MNP	Discovery Bay	14	_	-	-	17	20		-	
	Point Addis	35	-	-	-	41	49	-	-	
	Port Phillip Heads	31	-	-	-	35	49		-	

	Twelve Apostles	256	6		-	302	100	60	-
	Wilsons Promontory	23			-	26	22	-	-
MP	Lower South East	10	-		-	13	16	-	-
	Bunurong Marine Park	17	-	_	-	20	36	-	-
NP	Corner Inlet Marine and Coastal	10	-		-	11	2	-	-
	Wilsons Promontory Marine Park	23	-		-	27	8	_	-
	Corner Inlet	10	-		-	11	2	-	-
RAMSAR	Port Phillip Bay and Bellarine	19	-		-	25	39	-	-
	Western Port	21	-	-	-	24	19	-	-
	Phillip Island	30	-	-	-	35	46	-	-
	Mud Island	23	-		-	28	29	-	-
	Moncoeur Islands	12	-		-	14	14	-	-
	Rodondo Island	13	-		-	17	16	-	-
	Glennie Group	22			-	25	20	-	-
	Norman Island	24	_		-	28	15	_	-
	Shellback Island	23	-		-	27	6	-	-
	Kanowna Island	14	-		-	16	21		-
	Skull Rock	15	-		-	17	21		-
	Glenelg	36	-		-	41	45	-	-
SHORE	Warrnambool	34	-		-	38	63	-	-
ONORE	Moyne	82	1	_	-	90	95	-	-
	Corangamite	255	5		-	293	100	30	-
	Colac Otway	294	17	-	-	333	100	71	-
	Surf Coast	47	_		-	59	48		-
	Greater Geelong	46	_		-	52	44		-
	Mornington Peninsula	41	-		-	47	62		-
	Bass Coast	20	-		-	23	41		-
	South Gippsland	24	-		-	27	28	-	-
	Grant	10	-		-	14	16	-	-
	Lady Julia Percy Island	33	-		-	40	58	-	-
	Laurence Rocks	33	-		-	37	46		-
State	South Australia State Waters	13	-		-	22	17		-
Waters	Victoria State Waters	296	17	-	-	336	100	73	-

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	Corner Inlet	10	-	-	-	12	3	-	
	Wilsons Promontory (East)	11	-	-	-	14	17	-	
	Wilsons Promontory (West)	24	-	-	-	27	20	-	
	Waratah Bay	18	-	-	-	22	14	-	
	Cape Liptrap (NW)	20	-	-	-	24	28	-	
	Venus Bay	17	-	-	-	20	36	-	_
	Kilcunda	20	-	-	-	23	41	-	_
	French Island / San Remo	16	-	-	-	19	24	-	-
	French Island / Crib Point	9	-	-	-	12	9	-	-
	Westernport	25	-	-	-	29	42	-	
	Mornington Peninsula (S)	33	-	-	-	39	60	-	
	Mornington Peninsula (SW)	41	-	-	-	47	62	-	
	Port Phillip (Sorrento Shore)	41	-	-	-	45	53	-	
	Port Phillip (Mornington)	11	-	-	-	12	18	-	
	Port Phillip Heads	25	-	-	-	32	41	-	
SUB-LCA	Port Phillip (Queenscliff)	31	-	-	-	36	44	-	
SOD-LOA	Torquay	46	-	-	-	52	39	-	
	Anglesea	30	-	-	-	34	38	-	
	Lorne	48	-	-	-	59	48	-	
	Cape Patton	78	2	-	-	121	95	7	-
	Apollo Bay	80	4	-	-	139	95	17	
	Cape Otway West	294	17	-	-	333	100	71	
	Moonlight Head	255	5	-	-	293	100	30	-
	Port Campbell	155	3	-	-	196	100	27	
	Bay of Islands	82	1	-	-	90	95	-	
	Childers Cove	63	1	-	-	72	68	-	
	Warrnambool	28	-	-	-	34	56	-	
	Port Fairy	26	-	-	-	31	46	-	
	Portland Bay (East)	15	-	-	-	18	12	-	-
	Portland Bay (West)	22	-	-		25	19	-	-
	Cape Nelson	36	-	-	-	41	45	-	-
	Discovery Bay (East)	11	-	-	-	14	8	-	-

*Concentration recorded over a 48-hour window.

^Instantaneous concentration recorded over one hour.



 Table 26
 Predicted probability and maximum entrained hydrocarbon exposure (for 1 hour and 48-hour exposure windows) to individual receptors in the 0–10 m depth layer during winter conditions.

Receptor		Maximum time- entrained hydrocarbon	Probability of entrained hydrocarbon exposure for 48 hour window			Maximum entrained hydrocarbon exposure (ppb) for 1	Probability of entrained hydrocarbon exposure for 1 hour window		
	48 hour window		Low Moderate High		nour window	Low	Moderate	High	
AMP	Apollo	85	7			225	100	48	
	Beagle	18		-		24	40	-	
	King Island	10		-		14	10	-	
	Flinders	14		-	_	23	19	-	
IBRA	Warrnambool Plain	178	4	-	_	214	100	39	
	Otway Ranges	168	6	-	_	202	100	47	-
	Otway Plain	303	10	-	-	333	100	58	
	Gippsland Plain	55		-	-	67	83	-	-
	Strzelecki Ranges	22	_	-	-	25	54	-	-
	Wilsons Promontory	69		-	-	79	74	-	-
	Bateman	6		-	-	6	-	-	-
	Batemans Shelf	9		-	_	12	8	-	-
	Twofold Shelf	14		-	_	23	21	-	-
	Otway	569	42	_		932	100	100	-
IMCRA	Victorian Embayments	28		_	-	32	57	hour windo w Moderate 0 48 0 - 2 - 2 - 0 47 0 39 0 47 0 58 3 - 4 - 4 - 1 - 10 100 7 - 10 100 7 - 10 23 5 - 7 - 2 - 1 - 9 - $-$ - 6 - 2 - 9 - 00 43	-
	Central Victoria	112	7	_	-	225	100	48	-
	Central Bass Strait	105	4	_	-	227	100	23	-
	Flinders	72	-	-	_	84	75	Ability of entrearbon exposes Aur window Moderate 48 - - 39 47 58 - - 100 - 48 23 - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -	-
	West Tasmania Canyons	17		-		21	17	-	-
KEF	Bonney Coast Upwelling	32	1	_		42	32	Low Moderate 100 48 40 - 10 - 19 - 100 39 100 39 100 47 100 58 83 - 54 - 74 - - - 8 - 21 - 100 100 57 - 100 100 57 - 100 23 75 - 17 - 32 - 21 - 29 - - - 16 - 72 - 59 - 100 43	-
	Upwelling East of Eden	14		-	-	17	21	-	-
	Bunurong	11		-	-	15	29	-	-
	Cape Howe	9			-	9	-	-	-
	Churchill Island	rs72Tasmania Canyons17Py Coast Upwelling32ling East of Eden14ong11Howe9hill Island14Addis34		_	-	16	16	-	-
IVITNI	Point Addis	34		-	-	38	72	-	-
	Port Phillip Heads	25		-	-	30	59	-	-
	Twelve Apostles	169	6	-	-	230	100	43	-

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RPS

	Wilsons Promontory	71	-	-	-		74	-	-
AMP	Apollo	85	7	-	-	225	100	48	-
MP	Batemans	7	-	-	-	9	-	-	-
	Bunurong Marine Park	16	-	-	-	19	47	-	-
	Corner Inlet Marine and Coastal Park	10	-	-	-	12	10	-	-
	Shallow Inlet Marine and Coastal Park	10	-	-	-	12	9	- - - - - - - - - - - - - - - - - - -	-
	Wilsons Promontory Marine Park	60	-	-	-	67	72	-	-
	Corner Inlet	10	-	-	-	12	10	-	-
RAMSAR	Port Phillip Bay and Bellarine Peninsula	18	-	-	-	23	27	- 48 - - - - - - - - - - - - - - - - - -	-
	Western Port	16	-	-	-	21	30		-
RSB	New Zealand Star Bank	7	-	-	-	9	-	-	-
	King Island	10	-	-	-	14	10	-	-
	Seal Islands	7	-	-	-	11	2	-	-
	Phillip Island	28	-	-	-	33	79	-	-
	French Island	11	-	-	-	18	11	-	-
	Mud Island	15	-	-	-	19	25	-	-
	Curtis Island	8	-	-	-	11	5	-	-
	Moncoeur Islands	18	-	-	-	24	38	-	-
	Hogan Island Group	14	-	-	-	23	19	-	-
	Rodondo Island	19	-	-	-	25	59	-	-
	Glennie Group	68	-	-	-	78	74	-	-
SHORE	Norman Island	71	-	-	-	84	74	47 - 10 - 9 - 72 - 10 - 27 - 30 - 27 - 30 - 27 - 30 - 27 - 30 - 10 - 27 - 30 - 10 - 2 - 79 - 11 - 25 - 5 - 38 - 19 - 59 - 74 - 69 - 69 - 69 - 69 - 70 - 30 8 72 8 100 36 100 58 69 - 54 -	-
ONORL	Shellback Island	36	-	-	-	44	69		-
	Montague Island	6	-	-	-	9	-	-	-
	Anser Island	41	-	-	-	49	69	-	-
	Kanowna Island	36	-	-	-	42	69	-	-
	Skull Rock	37	-	-	-	42	70	-	-
	Warrnambool	80	-	-	-	137	30	8	-
	Moyne	143	4	-	-	207	72	8	-
	Corangamite	178	5	-	-	214	100	36	-
	Colac Otway	303	10	-	-	333	100	58	-
	Surf Coast	45	-	-	-	50	69	- - - - - - - - 8 8 - 8 - - - - - - - -	-
	Greater Geelong	45	-	-	-	51	54	-	-

RPS

	Mornington Peninsula	37	_	-	-	42	83	-	-
	Bass Coast	19	-	-	-	23	52	-	-
	South Gippsland	65	-	-	-	72	73	-	-
	Eurobodalla	6	-	-	-	9	-	-	-
	Lady Julia Percy Island	32	-	-	-	37	24	-	-
	Laurence Rocks	8	-	-	-	12	4	-	-
.	Tasmania State Waters	14	-	-	-	23	21	-	-
State Waters	Victoria State Waters	303	16	-	-	333	100		-
Waters	New South Wales State Waters	9	-	-	-	13	11		-
	Eurobodalla	6	-	-	-	9	-	-	-
	Corner Inlet	10	-	-	-	12	10	-	-
	Wilsons Promontory (East)	22	-	-	-	27	56	-	-
	Wilsons Promontory (West)	65	-	-	-	72	73	-	-
	Waratah Bay	22	-	-	-	25	54	-	-
	Cape Liptrap (NW)	27	-	-	-	31	66	-	-
	Venus Bay	16	_	-	-	18	45	-	-
	Kilcunda	19	-	-	-	23	52	-	-
	French Island / San Remo	13	_	-	-	15	28	-	-
	French Island / Crib Point	12	-	-	-	19	11	-	-
	Westernport	23	-	-	-	28	64	-	-
	Mornington Peninsula (S)	36	-	-	-	42	83	-	-
SUB-LGA	Mornington Peninsula (SW)	37	-	-	-	42	83	-	-
	Port Phillip (Sorrento Shore)	31	-	-	-	35	75	-	-
	Port Phillip Heads	24	-	-	-	29	46	-	-
	Port Phillip (Queenscliff)	29	_	-	-	36	50	-	-
	Torquay	45	-	-	-	51	34	-	-
	Anglesea	29	-	-	-	34	49	-	-
	Lorne	39	1	-	-	50	69	-	-
	Cape Patton	67	3	-	-	95	99	-	-
	Apollo Bay	70	4	-	-	132	100	11	-
	Cape Otway West	303	10	-	-	333	100	58	-
	Moonlight Head	178	4	-	-	214	100	36	-
	Port Campbell	127	3	-	-	182	91	11	-

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Bay of Islands	84	1	-	-	104	72	2	-
Childers Cove	143	4	-	-	207	46	8	-
Warrnambool	16	_	-	-	22	21	-	-
Port Fairy	12	-	-	-	16	14	-	-
Portland Bay (East)	9	-	-	_	11	2	-	-

*Concentration recorded over a 48-hour window.

^Instantaneous concentration recorded over one hour.



11 REFERENCES

- American Society for Testing and Materials (ASTM) 2013, 'F2067-13 Standard Practice for Development and Use of Oil-Spill Trajectory Models', ASTM International, West Conshohocken (PA).
- Andersen, OB 1995, 'Global ocean tides from ERS 1 and TOPEX/POSEIDON altimetry', Journal of Geophysical Research: Oceans, vol. 100, no. C12, pp. 25249–25259.
- Australian Maritime Safety Authority (AMSA) 2015a, Technical Guidelines for Preparing Contingency Plans for Marine and Coastal Facilities.
- Australian Maritime Safety Authority (AMSA) 2015b, National Plan Response, Assessment and Termination of Cleaning for Oil Contaminated Foreshores (NP-GUI-025)
- Becker, JJ, Sandwell, DT, Smith, WHF, Braud, J, Binder, B, Depner, J, Fabre, D, Factor, J, Ingalls, S, Kim, S-H, Ladner, R, Marks, K, Nelson, S, Pharaoh, A, Trimmer, R, Von Rosenberg, J, Wallace, G & Weatherall, P 2009, 'Global bathymetry and evaluation data at 30 arc seconds resolution: SRTM30_PLUS', Marine Geodesy, vol. 32, no. 4, pp. 355–371.
- Belore, UC 2014, Subsea chemical dispersant research. Proceedings of the 37th AMOP Technical Seminar on Environmental Contamination and Response, Environmental Canada, Canmore, Alberta, Canada pp 618-650.
- Bonn Agreement 2009, 'Bonn Agreement aerial operations handbook, 2009 Publication of the Bonn Agreement', London, viewed 13 January 2015, <u>http://www.bonnagreement.org/site/assets/files/3947/ba-aoh_revision_2_april_2012.pdf</u>
- Brandvik, PJ, Johansen, O, Leirvik, F, Farooq, U & Daling PS 2013, 'Droplet Breakup in subsurface oil releases Part 1: Experimental study of droplet breakup and effectiveness of dispersant injection', *Marine Pollution Bulletin*, vol. 73, no. 1, pp 319–326.
- Brandvik, PJ, Johansen, O, Farooq, U, Angell, G and Leirvik, F, 2014. Sub-surface oil releases Experimental study of droplet distributions and different dispersant injection techniques- version 2. A scaled experimental approach using the SINTEF Tower basin. SINTEF report no: A25122. Trondheim Norway 2014. ISBN: 9788214057393.
- Chassignet, EP, Hurlburt, HE, Smedstad, OM, Halliwell, GR, Hogan, PJ, Wallcraft, AJ, Baraille, R & Bleck, R 2007, 'The HYCOM (hybrid coordinate ocean model) data assimilative system', Journal of Marine Systems, vol. 65, no. 1, pp. 60–83.
- Chassignet, E, Hurlburt, H, Metzger, E, Smedstad, O, Cummings, J & Halliwell, G 2009, 'U.S. GODAE: Global Ocean Prediction with the HYbrid Coordinate Ocean Model (HYCOM)', Oceanography, vol. 22, no. 2, pp. 64–75.
- Condie, SA., & Andrewartha, JR (2008). Circulation and connectivity on the Australian Northwest Shelf. Continental Shelf Research, 28, 1724-1739.
- Davies, AM 1977a, 'The numerical solutions of the three-dimensional hydrodynamic equations using a Bspline representation of the vertical current profile', in JC Nihoul (ed), Bottom Turbulence: Proceedings of the 8th Liège Colloquium on Ocean Hydrodynamics, Elsevier Scientific, Amsterdam, pp. 1–25.



- Davies, AM 1977b, 'Three-dimensional model with depth-varying eddy viscosity', in JC Nihoul (ed), Bottom Turbulence: Proceedings of the 8th Liège Colloquium on Ocean Hydrodynamics, Elsevier Scientific, Amsterdam, pp. 27–48.
- DEWHA, 2007. Characterisation of the marine environment in the north marine region. Marine Division, Department of the environment, water heritage and the arts.
- DEWHA. 2008. The North-West Marine Bioregional Plan Bioregional Profile. Retrieved February 12, 2013, from Australian Government Department of Environment, Water, Heritage and the Arts: http://www.environment.gov.au/coasts/mbp/publications/north-west/pubs/bioregional-profile.pdf
- French, D, Schuttenberg, H & Isaji, T 1999, 'Probabilities of oil exceeding thresholds of concern: examples from an evaluation for Florida Power and Light', Proceedings of the 22nd Arctic and Marine Oil Spill Program (AMOP) Technical Seminar, Environment Canada, Alberta, pp. 243–270.
- French-McCay, DP 2003, 'Development and application of damage assessment modelling: example assessment for the North Cape oil spill', Marine Pollution Bulletin, vol. 47, no. 9, pp. 9–12.
- French-McCay, DP 2004, 'Spill impact modelling: development and validation', Environmental Toxicology and Chemistry, vol. 23, no.10, pp. 2441–2456.
- French-McCay, D, Rowe, JJ, Whittier, N, Sankaranarayanan, S, & Etkin, DS 2004, 'Estimate of potential impacts and natural resource damages of oil', Journal of Hazardous Materials, vol. 107, no. 1, pp. 11–25.
- Gordon, R 1982, 'Wind driven circulation in Narragansett Bay' PhD thesis, Department of Ocean Engineering, University of Rhode Island.
- Isaji, T & Spaulding, M 1984, 'A model of the tidally induced residual circulation in the Gulf of Maine and Georges Bank', Journal of Physical Oceanography, vol. 14, no. 6, pp. 1119–1126.
- Isaji, T, Howlett, E, Dalton C, & Anderson, E 2001, 'Stepwise-continuous-variable-rectangular grid hydrodynamics model', Proceedings of the 24th Arctic and Marine Oil spill Program (AMOP) Technical Seminar (including 18th TSOCS and 3rd PHYTO), Environment Canada, Edmonton, pp. 597–610.
- International Tankers Owners Pollution Federation (ITOPF) 2014, 'Technical Information Paper 2 Fate of Marine Oil Spills', International Tankers Owners Pollution Federation td, UK.
- Kostianoy, AG, Ginzburg, AI, Lebedev, SA, Frankignoulle, M & Delille, B 2003, 'Fronts and mesoscale variability in the southern Indian Ocean as inferred from the TOPEX/POSEIDON and ERS-2 Altimetry data', Oceanology, vol. 43, no. 5, pp. 632–642.
- Levitus, S, Antonov, JI, Baranova, OK, Boyer, TP, Coleman, CL, Garcia, HE, Grodsky, AI, Johnson, DR, Locarnini, RA, Mishonov, AV, Reagan, JR, Sazama, CL, Seidov, D, Smolyar, I, Yarosh, ES & Zweng, MM 2013, 'The World Ocean Database', Data Science Journal, vol.12, no. 0, pp. WDS229–WDS234.
- Li, Z, Spaulding, M, French-McCay, D, Crowley, D & Payne, JR 2017, 'Development of a unified oil droplet size distribution model with application to surface breaking waves and subsea blowout releases considering dispersant effects', *Marine Pollution Bulletin*, vol. 114, no. 1, pp 247–257.
- Ludicone, D, Santoleri, R, Marullo, S & Gerosa, P 1998, 'Sea level variability and surface eddy statistics in the Mediterranean Sea from TOPEX/POSEIDON data', Journal of Geophysical Research I, vol. 103, no. C2, pp. 2995–3011.



- Matsumoto, K, Takanezawa, T & Ooe, M 2000, 'Ocean tide models developed by assimilating TOPEX/POSEIDON altimeter data into hydrodynamical model: A global model and a regional model around Japan', Journal of Oceanography, vol. 56, no.5, pp. 567–581.
- National Oceanic and Atmospheric Administration (NOAA) 2013, 'Screening level risk assessment package Gulf state', Office of National Marine Sanctuaries & Office of Response and Restoration, Washington DC.
- Owen, A 1980, 'A three-dimensional model of the Bristol Channel', Journal of Physical Oceanography, vol. 10, no. 8, pp. 1290–1302.
- Qiu, B & Chen, S 2010, 'Eddy-mean flow interaction in the decadally modulating Kuroshio Extension system', Deep-Sea Research II, vol. 57, no. 13, pp. 1098–1110.
- Saha, S, Moorthi, S, Pan, H-L, Wu, X, Wang, J & Nadiga, S 2010, 'The NCEP Climate Forecast System Reanalysis', Bulletin of the American Meteorological Society, vol. 91, no. 8, pp. 1015–1057.
- Spaulding, ML., Kolluru, VS, Anderson, E & Howlett, E 1994, 'Application of three-dimensional oil spill model (WOSM/OILMAP) to hindcast the Braer Spill', Spill Science and Technology Bulletin, vol. 1, no. 1, pp. 23–35.
- Spaulding, MS, Mendelsohn, D, Crowley, D, Li, Z, and Bird A, 2015. Technical Reports for Deepwater Horizon Water Column Injury Assessment- WC_TR.13: Application of OILMAP DEEP to the Deepwater Horizon Blowout. RPS APASA, 55 Village Square Drive, South Kingstown, RE 02879.

Willmott, CJ 1981, 'On the validation of models', Physical Geography, vol. 2, no. 2, pp.184–194.

- Willmott, CJ 1982, 'Some comments on the evaluation of model performance', Bulletin of the American Meteorological Society, vol. 63, no. 11, pp.1309–1313.
- Willmott CJ, Ackleson SG, Davis RE, Feddema JJ, Klink, KM, Legates, DR, O'Donnell, J & Rowe, CM 1985, 'Statistics for the evaluation of model performance', Journal of Geophysical Research, vol. I 90, no. C5, pp. 8995–9005.
- Willmott, CJ & Matsuura, K 2005, 'Advantages of the mean absolute error (MAE) over the root mean square error (RMSE) in assessing average model performance', Journal of Climate Research, vol. 30, no. 1, pp. 79–82.
- Yaremchuk, M & Tangdong, Q 2004, 'Seasonal variability of the large-scale currents near the coast of the Philippines', Journal of Physical Oceanography, vol. 34, no., 4, pp. 844–855.
- Zigic, S, Zapata, M, Isaji, T, King, B, & Lemckert, C 2003, 'Modelling of Moreton Bay using an ocean/coastal circulation model', Proceedings of the 16th Australasian Coastal and Ocean Engineering Conference, the 9th Australasian Port and Harbour Conference and the Annual New Zealand Coastal Society Conference, Institution of Engineers Australia, Auckland, paper 170.